

MONTVILLE
North's South Center Road

18

FIELD BOOK

740

TABLE FOR REDUCING PERCHES TO FEET AND INCHES.

PERCH	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.	PERCH.	FEET.
1	16 6 in.	21	3 46 6 in.	41	6 76 6 in.	61	10 06 6 in.	81	13 36 6 in.				
2	33 0	22	3 63 0	42	6 93 0	62	10 23 0	82	13 53 0				
3	49 6	23	3 79 6	43	7 09 6	63	10 39 6	83	14 09 6				
4	66 0	24	3 96 0	44	7 26 0	64	10 56 0	84	14 26 0				
5	82 6	25	4 12 6	45	7 42 6	65	10 72 6	85	14 42 6				
6	99 0	26	4 29 0	46	7 59 0	66	10 89 0	86	14 59 0				
7	1 15 6	27	4 45 6	47	8 15 6	67	11 05 6	87	15 15 6				
8	1 32 0	28	4 62 0	48	8 32 0	68	11 22 0	88	15 32 0				
9	1 48 6	29	4 78 6	49	8 48 6	69	11 38 6	89	15 48 6				
10	1 65 0	30	4 95 0	50	8 65 0	70	11 55 0	90	16 05 0				
11	1 81 6	31	5 11 6	51	8 81 6	71	12 11 6	91	16 21 6				
12	1 98 0	32	5 28 0	52	8 98 0	72	12 28 0	92	16 38 0				
13	2 14 6	33	5 44 6	53	9 14 6	73	12 44 6	93	16 54 6				
14	2 31 0	34	5 61 0	54	9 31 0	74	12 61 0	94	17 11 0				
15	2 47 6	35	5 77 6	55	9 47 6	75	12 77 6	95	17 27 6				
16	2 64 0	36	5 94 0	56	9 64 0	76	12 94 0	96	17 44 0				
17	2 80 6	37	6 10 6	57	9 80 6	77	12 10 6	97	18 0 6				
18	2 97 0	38	6 27 0	58	9 97 0	78	12 27 0	98	18 17 0				
19	3 13 6	39	6 43 6	59	9 13 6	79	12 43 6	99	18 33 6				
20	3 30 0	40	6 60 0	60	9 30 0	80	13 0 0	100	19 0 0				

PLEASE RETURN TO
 GAUGA COUNTY ENGINEER
 COURT HOUSE
 CHARDON, O.
 PHONE 250-X

B. K. ELLIOTT COMPANY, PITTSBURG, PA.
 DRAWING MATERIALS AND SURVEYING INSTRUMENTS

GEAUGA COUNTY
 CHARDON, OHIO.

Property of
 County Surveyor's Office

NORTH and SOUTH
 CENTER ROAD, MONTVILLE TWP.

TOWNSHIP IMPROVEMENT.

B. R. Kenney
 Co. Sur. 1922

18

INDEX NEXT PG.

MIDDLEFIELD - MADISON RD.

Ohio #528 (thru Mont. Twp.)

Align & Structures 1-22

Profile 24-41

Topo 42-52

MONTVILLE DITCH 53-62

Montville School Board
Addition for filter bed (1955) 63-64

Abolition for filter bed (182) 63-64
Nicolville School Board

Sta Angle Bearing

11

10

9

8

7

6

5

4

3

2

1

0 Begin on Montville's S Line

N. 30°-57' E

7-6-'22
Fair-Fine

Hanna
Grou

Offset stakes set 20' Lt unless noted otherwise.

Note: This is not a survey of the actual Highway &. It locates merely the & for the placing of the Gravel Pavmt.

4+73

Lt end
10" x 10" Plank
Box

Red
12" Pipe

Rt. end
10" V.P.

11 3' x 9'



0+98 = 2 x 3 stone
Box

2 x parapet
50m
13 1/2 x 8-07

E. end = 3 x 3
cover partly planked
Pool, but may do

Nail in Lt
side T.P.

172
fence line

spike

MONTVILLE
Township Line
Huntsburg Twp.

Sta. Angle Bearing

20

+274 Δ 0°-0'

19

18

17

32.9

+67² Δ 1°-33' Rt.

16

15

14

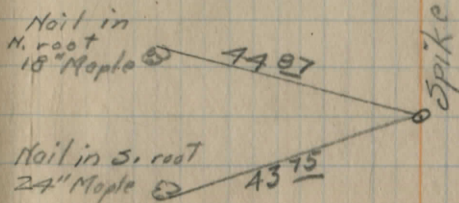
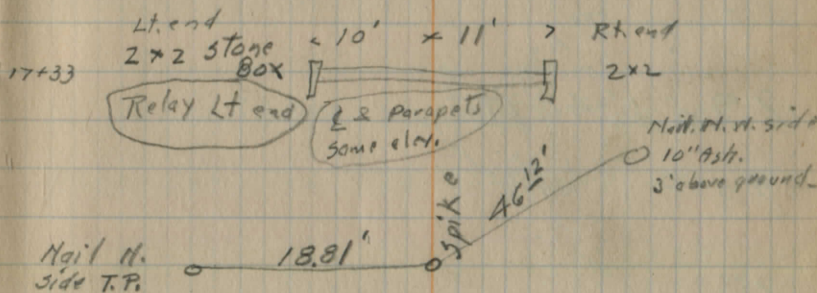
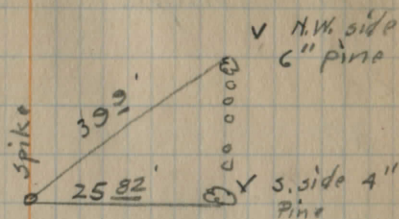
+81⁶ Δ 0°-0'

13

12

N. 5°-30' E

2



Hanna
Gro
Phillips

Sta. Angle Bearing
33

32+02

32

31

30 7-7-22 Fair
windy

29 Δ 1°-48' Lt.

28

27

26

25

24

23

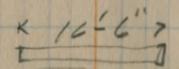
22

21

N 3°-42' E

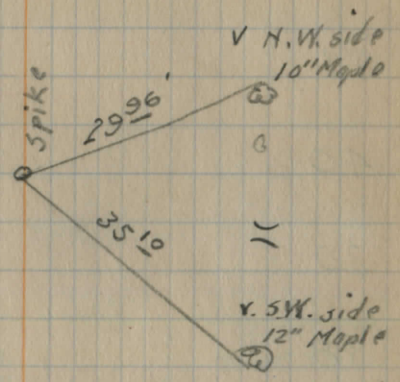
25+93 Rd to Lt.

12x12 plank box



Reqd 12" Pipe

(fd 1937)



Lt. end < 25+14 3 1/2 x 3 Stone Box



Good cond. O.K.

Head walls 2' high

Sta Angle Bearing

44

43

42

41

40

39

38

+46³ 0°-0'

37

36

+53⁵ 1°-30' Rt.

35

3A

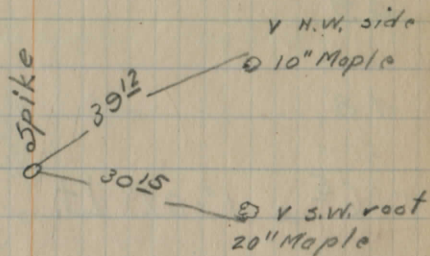
Con. Box G.K.

9.03

Spike

9.03

→



Sta Angle Bearing

P.M.
Moon
+74[±] Δ 3°-18' Rt.

(+45 N. Property Line - Brace on W. Katoлик on E.)

53

52

51

50

50 + 45

49 + 33

49

48

+06[±] Δ 1°-02' Lt.

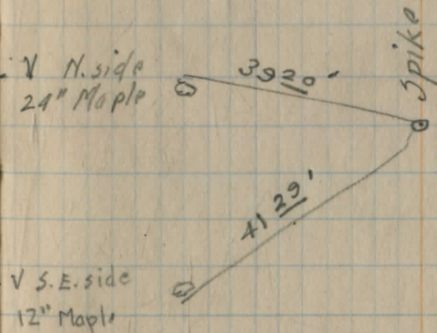
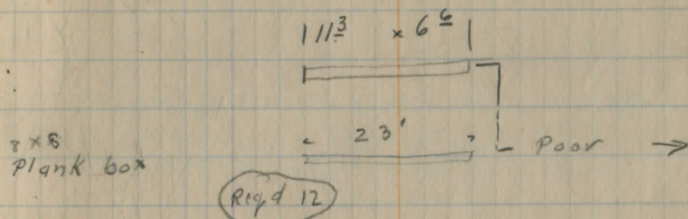
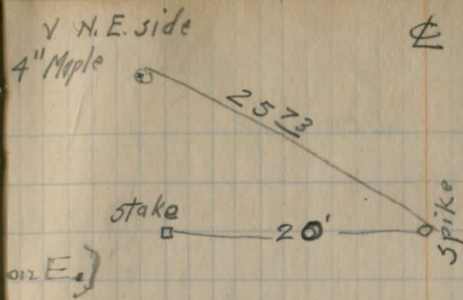
47

46

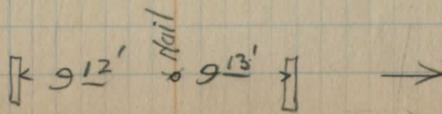
(+28 S. Prop. Line Brace - N; Katoлик E.)

45

+29[±] Δ 1°-09' Lt.



stone Box
OK,



sta. Angle Bearing

66

65

64

63

62

61

60

59

58

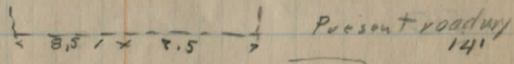
57

56

55

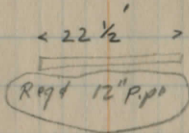
54

C5+44
 10' span Plank
 floor Brq.
 Stone abuts Good.
 make new 16' plank
 roadway



outlet, ditch needs
 cleaning out,
 clean out under Brq.

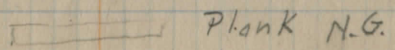
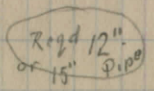
G1+02 1-5" x 6"
 Plank
 Poor Cond.



stone drain

offset 20' Rt.

55+07



Plank N.G.

Sta. Angle Bearing

79

78

77

76

75

74

73

72

71 \times $0^{\circ}-30'$ Rt.

Δ + 4 $\frac{1}{2}$ Rd to Rt. (Whitney Road)

70

69

68

67

79+85 $\frac{1}{2}$

old

plank Rd.

75+33 $\frac{1}{2}$ pipe

(clean outlet)

21'
10 + 12

old pipe
may do

offset stake \square 20' 0 spike

Ret. stake
at end of
corn row

Sta. Angle Bearing

92

91

90

89 Δ 0°-16' Rt.

88

87

86

85

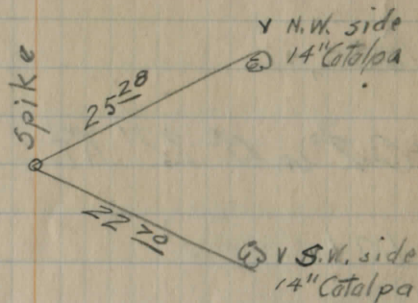
84

83

82

81

80



21400 10x10" Plank Box \sim 20' \sim Poor cond. (Reqd 12" pipe)

80105 9x9" plank Box \sim 18' \sim 10' \sim Looks good.

Sta. Angle Bearing
 $+71^{\circ} \triangle 0^{\circ}-0'$

104

103

102 $\triangle 0^{\circ}-22'$ Rt.

101

100

99 + 55

99

98

97

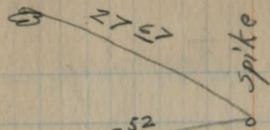
96

95

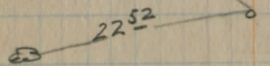
94

93

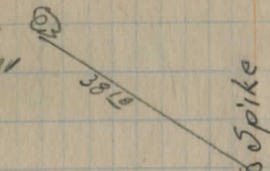
v. N.E. side
 12" Ash.



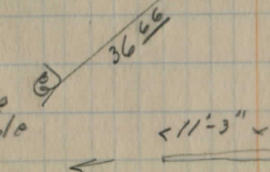
v. s. side
 Triple Ash



v. s. side
 4" Poplar



v. s. side
 14" Maple



$\langle 11'-3" \sim 11'-3" \rangle$

O.K.

Sta. Angle Bearing

11c
+40' 0°-0'

115

114

113

112

111

110

109

108

107

106

105

v N. side
10" Maple 29'10"

v SE side
9" Whitewood 34'22"

113+5C
12" v.P.
(Red 12" coppice)

← 12'-6" × 8'-0" →

Rt. end Bucken

110+50

12" CW No. 6 Stone drain

could be omitted if
water is taken to North

← 9'-0" × 22'-6" →

3×4
108+05 Stone Box

Extend Lt End
relay Lt. end 6'

±

10

Sta Angle Bearing

128

127

+397 Δ 1°-16' Lt.

126

125

124

123

122

121

120

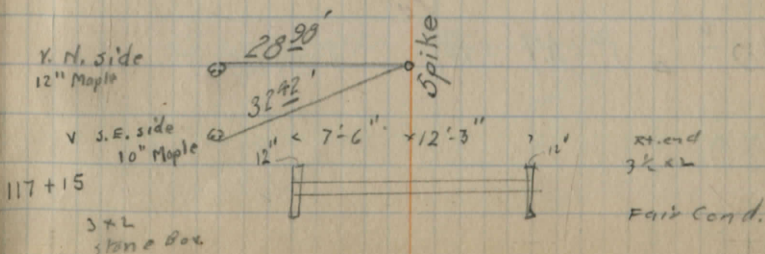
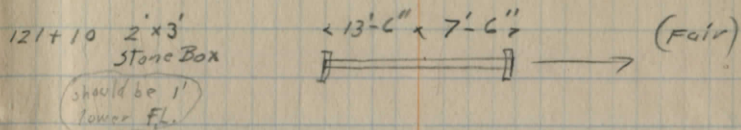
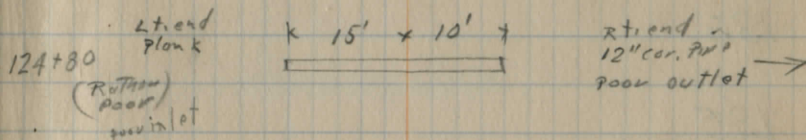
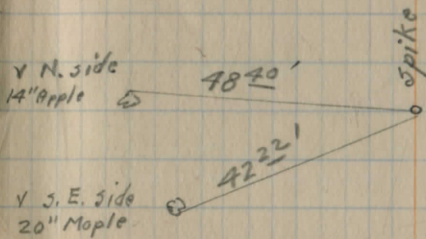
119 Δ 0°-0'

118

117

±

11



Sta Angle Bearing
 +70 0°-21' Lt

139

138

137

136

135

134

133

132

131

+18⁶ 1°-47' Rt

130

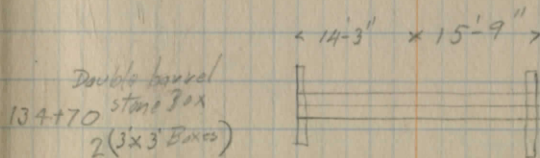
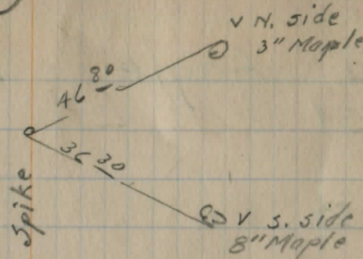
129

24 1/2 Miles

7-10-'22
 Hot, Windy

Hanna
 Grad
 Sperry

12



131 offset 40' Lt
 38' Lt

10' Concrete Pavement

30⁰⁰
 spike
 Offset 130, 20' Rt

sta Angle Bearing

151

150

149

148

147

146

$+73^{\circ} 5' \triangle 0^{\circ} 29' \text{ N.}$

145

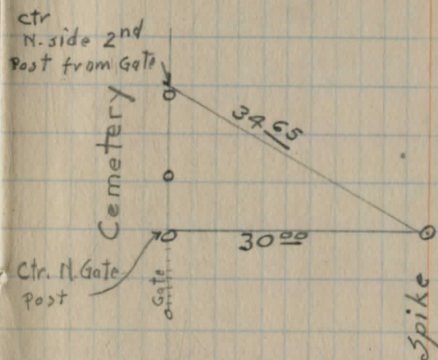
144

143

142

141

140



Sta. Angle Bearing

163

162 Δ $0^{\circ}-14'$ Lt.

161

160

159

158

$+58^{\circ}$ Δ $0^{\circ}-0'$

157

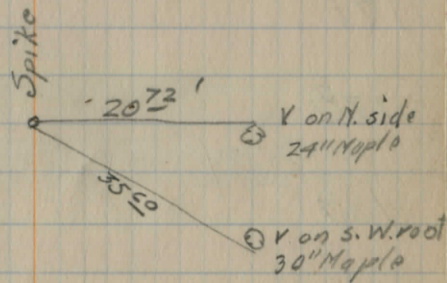
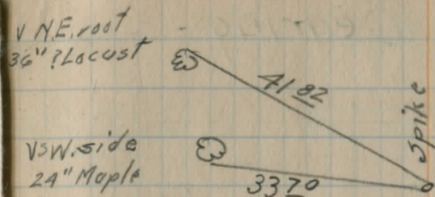
156

155

154

153

152



Sta Angle Bearing

176

175

174

173 Δ 0°-0'

172

171

170

169

168

167

166

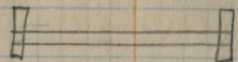
165

164

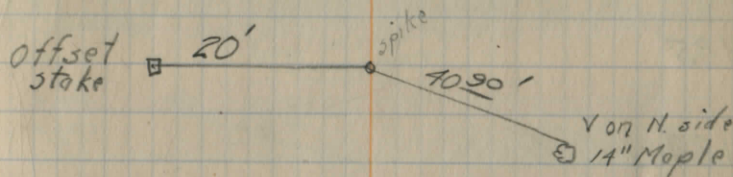
15

174+97
2x2 L head
stone box
(2 1/2 ft end)

<12'-6" x 8'-6">

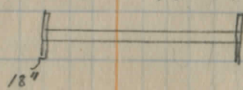


Damed up for
Duck Pond →
culv. full of water



169+34
4' x 3 stone box
Extend Lt. end

<6'-5" x 13'-4">



outlet filled →
100' Rt.
1 1/2' mud in culv.

Sta Angle Bearing

188

187

186

185

184 Δ 0°-0'

183

182

181

180

179

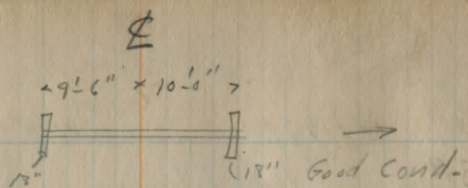
178

+22⁹ Δ 0°-0'

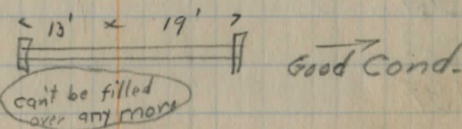
177

188+90

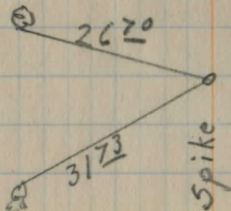
3' x 3' Stone Box



185+69
2' x 3' Stone Box



v s. side
12" Apple



v N.W. side
2" W. Cherry

Spike

29⁹⁷

v N. side 2"
cherry

45²⁷

v N.E. side
20" Cherry

Sta. Angle Bearing
 +25° 6°-10' Rt.

200

199 0°-0'

198

197

196

195

194

193

192 +20 E Rd Lt.
 775 191+82 & Rd Rt.

+22° 0°-0'

(None set)
 191+50 offset 20' Lt.

191

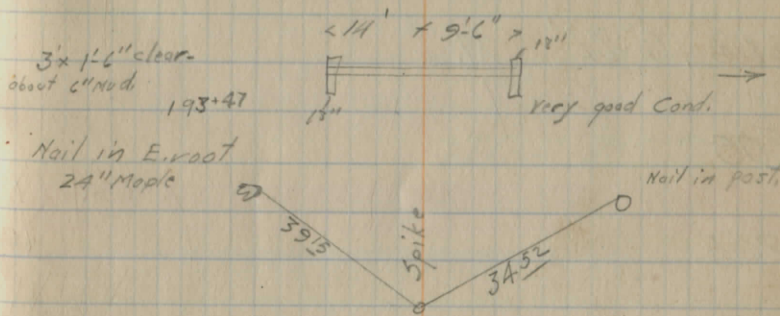
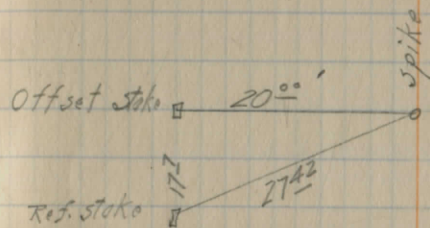
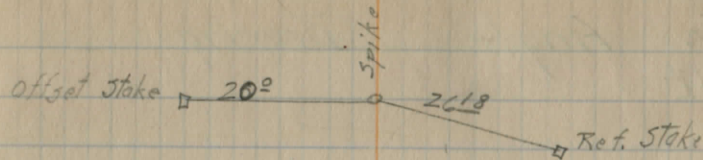
190

189

7-12-22 Hot Windy

Hanna
 Grad.
 Sperry

17



Sta. Angle Bearing

212

211

210

209

208

207

+24° 0°-22' Rt.

206

205

204

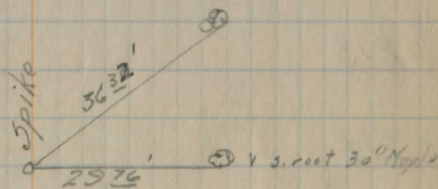
203

202

201

8

13



offset 20' Rt.

202+06
37x3
stone Box



culv. fair except ends -
Relay each end -

Sta Angle Bearing
223

+54⁶ 0°-10' Lt.

222

221

220

219

218

+05⁵ 0°-22' Lt.

217

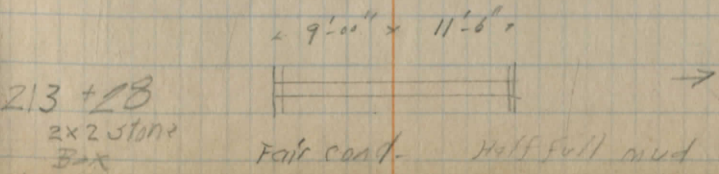
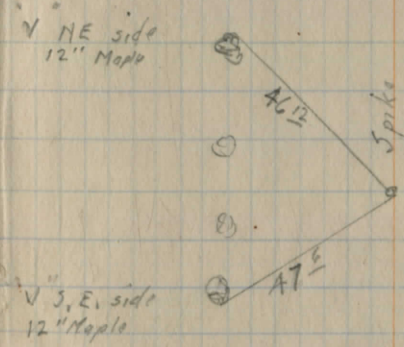
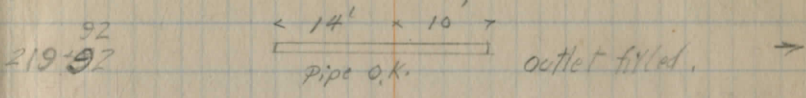
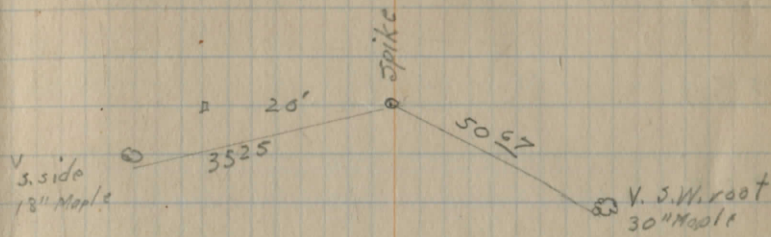
216

215

214

213

⊥



7-13-22 cloudy
cool

Sta. Angle Bearing

235

234

233

232

231

230

229

228

+31³ 0° 13' Rt.

227

226

225

224

Hanna
Grau
Sperry

20

< 17' x 13' >

234+61



234+25 ± Rd Lt

Lrd Rt, 234+40 (234?)

234+00



24" sec C.I.P. OK. < 27'-0" x 5'-6" > → Ext Rd. end

< 8' x 8' >

Iron Bridge
Plank floor 12 1/2
4.3' down to center
bottom, from bottom
of girder



Nail in
1st plank
3. end org.

(fair cond
will do)

→

Sta. Angle Bearing

247

246

245

244

243

242

241

240

+40° 0°-0'

239

238

237

236

28' x 7' x

245700
Plank Brg.

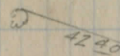
95.6"



stone Abuts

Good cond. →

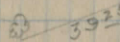
V N.E. side
24" Maple



4240

Spike

V S.E. side
12" Maple



3925

Sta.	Angle	Bearing
------	-------	---------

486 Mi.

+98° Montville's N. Line (approx)

256

(What Sta. res.)

255+87 2 1/2 x 3 Stone Box

<12'-0" x 12'-0">

Excellent Cond.

255

V N.E. side 12" Maple

2720

253+80

254 = 0° 5'

V S.E. side 12" Maple

2250

Pipe fd 5/4/37 S.W. set at same references

253

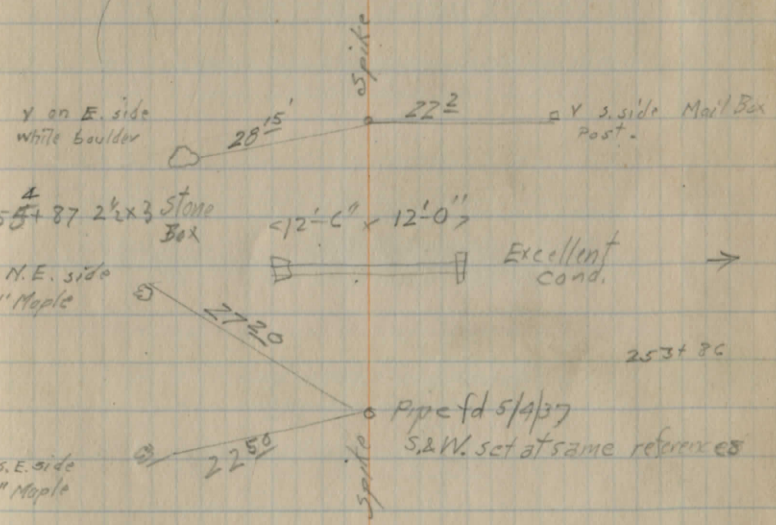
252

251

250

249

248



Sta Angle Bearing

- LEVELS -

7-13-22

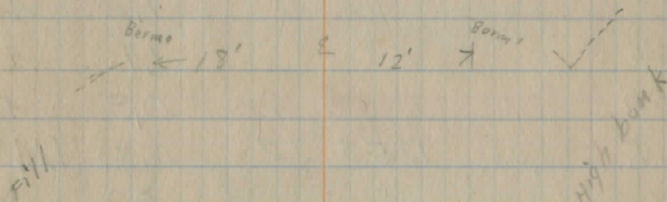
24

	B.S.	H.I.	F.S.	Elev.
B.M.	1.50	1211 01		1209.51
130+18 ^E			4.01	07.00
128 ^E			4.16	06.85
+33			5.2	05.8
131			5.6	05.4
132			7.1	03.9
+75			8.0	03.0
133			9.0	1202.0
134			13.1	1197.9
T.P.	9.70	1208 38	12.33	1198.68
+70			10.7	1197.7
B.M.			10.55	1197.83
135			10.1	1198.3
136			8.3	1200.1
137			3.8	1204.6
T.P.	11.20	1219 23	0.35	1208.03
138			7.7	1211.5
+35			4.2	15.0
139			0.9	18.3
T.P.	10.86	1230 03	0.06	1219.17
+50			8.9	21.4
140			7.2	22.8
141			4.2	25.8
142			2.3	27.7
T.P.	11.20	1240 73	0.50	1221.53

On N. root of maple Lt., & S. of Con Pav.
S. edge Con. 475" B"

Broad Rwy

No more fill over culv.
N.W. cor. W. Abut.



End Fill

End Bank

B. - 7.5 15.5 4.00
con + Walk 7.5 15.5

1240 73 ✓

143			9.7	31.0 ✓
144			6.5	34.2 ✓
U.S.G.S. B.M.			2.41	4238.25 1238.32 ✓
+20			5.2	35.5 ✓
145			3.0	37.7 ✓
175			1.4	39.3 ✓
146			0.7	40.0 ✓
T.P.	9.11	1249	0.20	64 ✓ 1249.53 ✓
147			8.3	41.3 ✓
148			7.0	42.6 ✓
149			5.9	43.7 ✓
150			5.0	44.6 ✓
151			3.5	46.1 ✓
152			1.8	47.8 ✓
153			1.7	47.9 ✓
154			1.4	48.2 ✓
155			0.9	48.7 ✓
T.P.	6.08	1255	0.33	^A ✓ 39 ✓ 1249.31 ✓
156			5.0	50.4 ✓
157			4.2	51.2 ✓
B.M.			2.66	1252.73 ✓
157+40			4.1	51.3 ✓
158			4.9	50.5 ✓
159			6.4	49.0 ✓
160			8.8	46.6 ✓

B < 11' + 12' > B

con A.W.K.

B < 11'-6" x 9'-6" > B

No. 8011K-5

B < 10' x 9' > B

Nail W. root Maple Rt. 1574 55

1255 39

161				10.2	45.2 ✓
162			0 ✓	11.3	44.1 ✓
T.P.	1.31	1245	79	10.91	1244.48 ✓
163				4.3	41.5 ✓
164				7.6	38.2 ✓
165			7 ✓	11.9	33.9 ✓
T.P.	0.93	1233	65	13.07	1232.72 ✓
166				3.7	30.0 ✓
167			✓	8A	25.3 ✓
T.P.	1.29	1222	64	12.30	1221.35 ✓
168				3.2	19.4 ✓
169				4.9	17.7 ✓
col. &				5.5	17.1 ✓
170				6.1	16.5 ✓
+30				6.1	16.5 ✓
171			✓	4.1	18.5 ✓
T.P.	6.62	1228	73	0.53	1222.11 ✓
B.M.				2.39	1226.34 ✓
172				5A	23.3 ✓
+60				3.4	25.3 ✓
173				4.1	24.6 ✓
+70				9.2	19.5 ✓
174				10.2	18.5 ✓
175 &				11.0	17.7 ✓
CUL,				9.5	19.2 ✓
+50					

3 or 2' Banks

B < 2.5 2.5 > B

B < 5' x B' > B

Banks end at +50

← about 1" fill

← flat →

11. W. side apple Rt. 172 + 05

3' Banks B - 9' x 9' > B 3' Bank

8' " " " 5' "

1' " " " 1' "

make no fill

1228 73 ✓

176			7.5	21.2 ✓
177			1.1	27.6 ✓
+25			0.2	28.5 ✓
T.P.	106	1229	0.44	1228.29
178			1.8	27.6 ✓
179			2.5	26.9 ✓
180			2.8	26.6 ✓
181			3.8	25.6 ✓
182			5.0	24.4 ✓
183			6.8	22.6 ✓
+60			7.7	21.7 ✓
184			10.0	19.4 ✓
T.P.	2.60	1219	5.9	1216.99
185			7.2	12.4 ✓
+70 & colv.			8.5	11.1 ✓
Lt. Par.			12.10	07.49 ✓
Rt. Par.			10.0	09.6 ✓
186			8.7	10.9 ✓
+60			7.5	12.1 ✓
187			5.1	14.5 ✓
+25			3.5	16.1 ✓
188			6.3	13.3 ✓
colv			6.7	12.9 ✓
189			7.0	12.6 ✓
190			6.4	13.2 ✓

Beams 10' 11' > Beams

2' bank beam 7' 14' > beam 1' bank

3' bank 8' < 6' 10' 7' 3' bank

end banks, begin fill
(don't fill)

Lt. (17.6 FL) hole 1202.0

Rt. (17.0 FL) 1202.6

fill < 6' * 12' > fill

4' Bank

< 7' * 11' >

(don't fill)

4' Bank

✓

1219 59

191			4.5	1215.1
192			2.2	1217.4
B.M.	3.90	1222 01	1.48	1218.11
193			4.5	17.5
culv			4.0	18.0
194			4.9	17.1
195			4.6	17.4
196			3.7	18.3
197			3.1	18.9
+50			3.5	18.5
198			4.8	17.2
199			6.3	15.7
200			10.0	12.0
T.P.	1.17	1214.28	8.90	1213.11
+25			3.9	1210.4
201			11.4	1202.9
T.P.	4.30	1205 70	12.58	1201.40
202	² culv		8.5	11.97.2
			13.1	1192.6
			14.0	1191.7
203			8.3	1197.4
204			3.2	1202.5
T.P.	11.87	1217 58	9.01	1205.69
+75			8.9	1208.7
205			8.0	1209.6

7-14-22
FairHanna
Grove
Phillips

28

12" Bank < 8' x 10' 6" > Berme 18" bank
 12" Bank < 8' x 10' 6" > Berme 18" bank
 E root Maple Lt. 1914 50
 Berme < 14' x 8' > Berme
 Level < 8' x 10.5' x 9' > 8' Level
 3' Bank < 6' x 8' > 3' bank
 6' bank < 9.5' x 4' > 8' c'bank
 Fill < 8' x 5' > 8' Fill
 Head wall Lt. $\frac{12.1}{18.8}$ FL Lt. 1186.9
 Head wall Rt. 20.0 FL Rt. 1185.7
 End of fill
 8' Bank < 8' x 6' > 8' bank

206			2.8	14.8
+15			2.6	15.0
+75			7.5	10.1
207			9.1	1208.5
208			12.0	1205.6
T.P.	3.91	1209	60 [✓]	11.89 1205.69 [✓]
B.M.			9.76	1208.4
209			5.6	1204.0
210			7.2	1202.4
211			10.1	1199.5
212			13.6	1196.0 [✓]
T.P.	6.98	1202	85 [✓]	12.83 1196.77 [✓]
213			8.5	1194.3
Culv.			8.6	1194.2
B.M.			7.58	1195.27
			10.9	1192.0
214			8.4	1194.4
+70			5.3	1197.5
215			4.6	1198.2
216			3.7	1199.1
217			1.8	1201.0
218			3.0	1199.8
+60			4.2	1198.6
219			8.0	1194.8
+40			11.2	1191.6 [✓]
T.P.	9.34	1193	97	9.24 1193.61 [✓]

9' x 6' 78 4' Bank

Wroot 18" Maple Rt. 208+50

1' bank < 7 1/2 x 7 1/2 > 1' bank

N.E. cor W. par

Fl. Lt. dirt

Bank 13' x 4 1/2 x 13' 70

No bank < 6 1/2 x 11' > No bank

1193 97

220			4.0	1190.0
221			5.3	1188.7
222			4.7	1189.3
+25			4.5	1189.5
+60			5.5	1188.5
223			7.7	1186.3
224			13.0	1181.0
TP ₁	0.70	1182 12	12.55	1181.42
+60			4.4	1177.7
225			8.9	1173.2
+25			11.0	1171.1
226			13.9	1168.2
T.P.	3.55	1172 59	13.08	1169.04
227			5.3	1167.3
Brq.			4.95	1167.64
J.M.			5.65	1166.94
228			5.0	1167.6
229			4.5	1168.1
230			4.4	1168.2
+50			4.0	1168.6
231			4.5	1168.1
TP ₁	3.95	1171 11	4.53	1168.06
232			3.8	1167.3
233			4.2	1166.9
234			5.4	1165.7

< 10' x 9' >

bank

Level < 6' x 10' > Level

Brq floor

S.W. cor. N. Abut. x

3' Bank to yard < 4' x 13' >

9 93

< 11 x 11 >

Lot 1

< 20' x 8' >

1171 11

culv →
235

5.5 656

6.0 65.1

236

5.7 65.4

237

4.2 66.9

238

0.6 70.5

T.F.

3.34 1172 36

1.09 1170.02

+30

2.3 71.1

239

6.2 67.2

+50

9.7 63.7

240

12.2 61.2

T.F.

1.95 1162 28

13.03 1160.33

241

3.9 58.4

242

6.0 56.3

243

7.9 54.4

244

8.6 53.7

245

7.9 54.4

B.M.

9.11 1153.17

246

8.4 53.9

247

6.1 56.2

T.F.

5.91 1161.54

6.65 1155.63

248

4.8 1156.7

249

4.6 1156.9

250

4.8 1156.7

✓

< 11' > 11' >

8' 9'

6' 10'

2' bank

- 4' - 10'

2' bank

- 4' - 11' -

Level

8 12

Level

" 10 - 14 "

Brq. floor

W. End H. Abut SW. Cor.

3' ditch

12 " "

1161 54

251			5.0	1156.5
252			4.2	1157.3
253			3.1	1158.4
#85			0.9	1160.6
254		✓	1.4	1160.1 ✓
T.P.	2.38	1163 08	98.7	1160.70
Culy.	(What Sta?)		4.8	1158.3
B.M.			3.18	1159.90
255			5.3	1157.8
256			4.5	1158.6
+98°			1.2	1161.9

S.W. Cor W. Par.

END

✓

B.M.	5.77	1215.20 ^v		1209.51
130			91	1206.2
129			5.7	1209.6
+80			4.8	1210.5
+30			0.5	1214.8
T.P.	9.80	1224.76 ^v	0.32	1214.96
128			8.5	1216.3
127			3.9	1220.9
+55			3.0	1221.8
+25			3.9	1220.9
126			5.3	1219.5
+70			7.4	1217.4
125			8.8	1216.0
+25			8.5	1216.3
124			7.7	17.1
+40			4.7	20.1
123			5.3	19.5
122			9.9	14.9
+50			10.3	14.5 ^v
T.P.	10.50	1226.48 ^v	8.78	1215.98
culy.			10.9	15.6
121			10.6	15.9
120			8.0	18.5
119			3.1	23.4
+50			5.1	21.4

7-14-22 P.M.
Fair

33

£

2' bank < 13'

- 13
+ 9

7' bank

> bank

8' bank

bank < 13'

11'

> bank

No banks

no banks.

< 11k

> 14

>

Fill

3' bank

< 8'

> 8'

> 4' bank

< 6'

> 10'

✓

122648

118			7.9	18.6
culv			8.1	18.4
B.M.			6.80	1219.68
117			8.5	1218.0
+25			7.5	1219.0
116			6.2	20.3
+40			3.0	23.5
115			4.3	22.2
114			6.9	19.6
T.P.	8.94	1228.08	7.34	1219.14
113			8.5	1219.6
112			5.7	22.4
+55			4.3	23.8
			1.77	10.4
111			4.7	23.4
110			3.8	24.3
+25			1.2	26.9
109			2.3	25.8
+40			6.2	21.9
108			7.5	20.6
			9.5	18.6
			16.3	11.8
culv.			7.3	20.8
107			4.8	23.3
T.P.	12.94	1240.80	0.27	1227.01

39

banks				banks
X N.W. cor				W. Par
2' fill				2' fill
bank	< 5k	x 15'	>	bank
2' bank	< 8	x 11'	>	
				3' bank
		13'	4' >	2' bank
				Bottom of slope on Rt.
		< 14	6'	>
		< 10	12'	>
10' bank				
		2'	15'	
		< 2'	15'	>
Lt. headwall				
FLILT				
		< 4'	17'	>

1240.80

106			7.1	1233.7
T.P.	11.92	1252.44 [✓]	0.28	1240.52
+10			11.8	40.6
105			11.3	41.1
104			8.1	44.3
103			5.2	47.2
+50			3.8	48.6
102			3.3	49.1
101			2.8	49.6
100			2.3	50.1
99			1.3	51.1
98			0.7	51.7 [✓]
T.P.	6.18	1257.99 [✓]	0.63	1251.81
B.M.			5.11	1252.88
97			5.3	52.7
96			4.4	53.6
95			4.5	53.5
94			4.5	53.5
93			3.5	54.5
+25			2.5	55.5
92			2.9	55.1
91			3.5	54.5
90			3.7	54.3
89			4.1	53.9 [✓]
T.P.	2.41	1256.44 [✓]	3.96	1254.03 [✓]

35

3' bank < 11 1/2' x 7' > 10' bank

- End bank < 72' 7' > end bank

< 9' x 8' >

< 9' x 8' >

- < 8' x 12' > Level

W. root 12" Maple Rt. 97+75

< 8' x 12 1/2' >

Level

1256 44

88			2.4	54.0
87			3.6	52.8
86			4.1	52.3
J.M.			2.25	1254.19
+55			5.3	51.1
85			7.9	48.5
84			9.4	47.0
83			10.4	46.0
82			10.7	45.7
81			10.8	45.6
T.P.	0.98	1246 65	10.77	1245.67
cult			2.1	44.5
80			2.4	44.2
79			3.9	42.7
78			4.9	41.7
77			5.1	41.5
76			5.5	41.1
2 Pipe			5.7	40.9
75			5.6	41.0
74			5.0	41.6
73			3.7	42.9
72			2.3	44.3
T.P.	2.60	1246 95	2.30	1244.35
71			1.9	45.0
+50			2.5	44.4
70			4.1	42.8

E. root 30" Maple Lt. 86+60

< 8' x 12' >

Level < 12 1/2' x 10 1/2' > Level

< 13' x 5' >

< 12 1/2' x 8' >

2' bank < 11' x 9' > 2' bank

1246 95

69			8.4	38.5
68			11.9	35.0
67			14.5	32.4
T.P.	0.17	1235.46	11.66	1235.29
66			4.1	1231.4
			4.4	31.1
B.M.			5.38	1230.02
65			6.1	29.4
64			6.7	28.2
+50			6.1	29.4
63			6.8	28.7
62			7.2	28.3
61			6.8	28.7
60			6.3	29.2
59			4.8	30.7
TP	10.36	1241.85	3.97	1231.49
58			9.7	32.1
+75			9.4	32.4
57			11.2	30.6
56			11.8	30.0
55			10.3	31.5
54			7.5	34.3
53			2.5	39.3
+50			1.2	40.6
52			3.3	38.5
51			6.4	35.2

Plank floor Dry,
x N.W. cor s. Abut.

< 10 1/2 x 11 1/2 >

< 13 x 14' >

< 14 1/2 x 8' >

< 11' x 7' >

2'-bank < 7 1/2 x 7 1/2 > #0 bank

1241 85

Pipe			7.3	34.5
50			7.1	34.7
49			7.0	34.8
48			5.5	36.3
T.P.	5.68	1242 07	5.46	1236.39
47			2.8	39.3
46			7.0	35.1
45			11.2	30.9
culv.			12.8	29.3
B.M.	7.50	1238 11	11.46	1230.61
44			10.2	27.9
43			9.9	28.2
42			8.4	29.7
41			5.5	32.6
+36			1.7	36.4
40			0.7	37.4
B.M.	7.81	1245 36	0.56	1237.55
39			6.2	39.2
+30			4.0	41.4
38			1.9	43.5
T.P.	3.70	1247 87	1.19	1244.17
+45			1.7	46.2
37			3.7	44.2
+75			5.5	42.4
36			8.0	39.9
35+53			8.2	39.7

7-17-22

Hanna
Graw
Sperry

38

4' bank	< 9 1/2	x	9 1/2	>
3' "				
x N.W. Cor W. Par				
1' F.V.I.	< 6	< 10	>	x fill
Level				Level
"	< 7	x 12'	>	"
3' bank				3' bank
bank				
4' bank				Level
W. root 15" Maple Rt. 40+06				
Level	< 13'	x 9'	>	Level

1247 87

B.M.				6.88	1240.99
35				7.9	40.0
+50				6.6	41.3
34				4.2	43.7
T.P.	11.49	1258.35		1.01	1246.86
33				9.4	48.9
32				9.8	48.5
31				8.8	49.5
30				7.6	53.7
29				7.0	54.3
+75				4.5	53.8
28				6.3	52.0
27				11.5	46.8
T.P.	6.22	1252.62		11.95	1246.40
+50				8.2	44.2
26				8.8	43.8
+50				9.4	43.2
culv				8.6	44.0
B.M.				6.52	1246.10
25				8.7	43.9
+50				8.4	44.2
24				7.6	45.0
23				4.1	48.5
22				1.5	51.1
T.P.	10.48	1262.45		0.65	1251.97

N.W. Cor. W. Par.

2' bank < 6' x 10' 1' bank
 about 1' fill
 < 8' x 11' >

level

5' bank

Level

x S.W. Cor. W. Par.

4' bank < 8' x 13' > Level
 " " " "

✓

1262 45

21			9.1	1253.3	
20			6.3	56.1	
+25			3.7	58.7	
19			4.7	57.7	
+50			7.4	55.0	
18			8.4	54.0	
cut			8.1	54.3	
B.M.			8.25	1254.20	
17			7.6	54.8	
+60			6.2	56.2	
16		✓	3.8	58.6	
T.P.	12.89	1274	76	0.58	1261.87
15			6.7	68.1	
+55			3.1	71.7	
14			1.0	73.8	
+70			0.7	74.1	
13			2.0	72.8	
12			3.5	71.3	
11			4.5	70.3	
T.P.	0.17	1270	53	4.40	1270.36
10			1.4	69.1	
9			3.4	67.1	
+40			5.3	65.2	
8			7.1	63.4	
7			9.3	61.2	

✓

40

Level < 14 x 12' > Lev

2' bank - 11 1/2 x 13' > 2' bank

Level

(Make no fill)

x N.W. Cor W. Par

3' bank - 11' x 7' > 3' bank

4' " 3' bank

4' " 1' bank

4' " - 11' x 11' > Level

3' "

1' "

Level

Level < 10 1/2 11 1/2 > Level

Level

3' bank < 10 x 10' > 3' bank

Level

1270 5-3

C			10.3	1260.2
Pipe			10.6	1259.9
5			11.0	59.5 ✓
T.P.	3.03	1262.56 ✓	11.00	1259.57
+60			3.4	59.2
4			5.5	57.1
+50			8.9	53.7
3			10.9	51.7
2			12.8	49.8
Culv. & /			13.4	49.2
B.M.			12.57	1249.99
+50			12.4	50.2
0			10.9	52.2
0-85			7.2	55.4

✓

about 1' fill

Level

Level

1' bank

- 9' x 8' >

1' bank

2' "

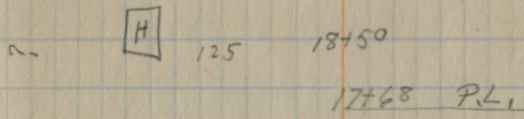
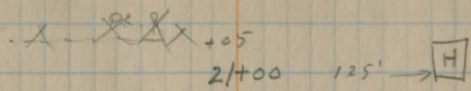
2' "

Level

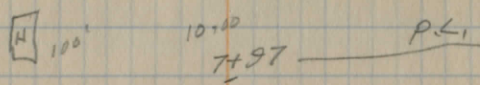
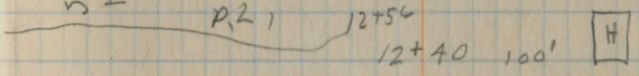
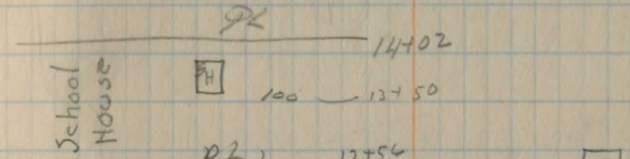
- 9' x 8' >

A Cor. W. Par.

Topo.



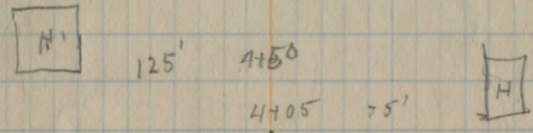
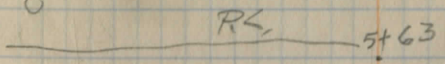
Baras?



Stelichy

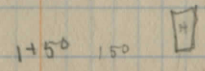
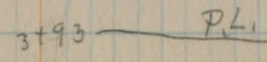
Chas. Lansky

Alec Seze



C. A. Rhodes

J. Schurmer



P. Szeszak

Two Line 0+00

Brace

P.L. 53+45 P.L.

52+55 60' [H]

P.B

[H] 200 49+75

P.L. 45+28 P.L.

J. Kradolik

M. Pecuzek

[H] 200 39+50

37+35 75' [H]

P.L. 35+62 P.L.

F. E. Bill

A. J. Cromwell

[H] 75' 33+10 40' [H]
32+70

30+70 80' [H]

H. A. Batchelder

30+60 P.L.

28+30 100 [H]

Rd.
Hautia
J. Hautala

[H] 100

25+60

P.L. ✓ 24+55

23+02 P.L.

Mrs. Culbertson

W.E. Kennerly

[H]

75

57+50

59+00

150'

[H]

69+75

[H]

61+90

PL

S. Rhodes

70+41

applied
K. P. G. Grant
5-22-29

J. Batchelder

79+75

30°

[H]

76+84

PL

W.F. Marquette

Bank Rd

81+21

Geo. Blaxter L. Wenzel

[H]

100

85+50

PL

82+15

93+56

PL

99+60

75'

[H]

[H]

60'

101+83

101+89

102+60

100'

[H]

P. Speck

off. ket

[H] 80' 126+95

M. Alvard 126+34

[H] 80' 25+96

F. Williams → PL 124+74 124+98

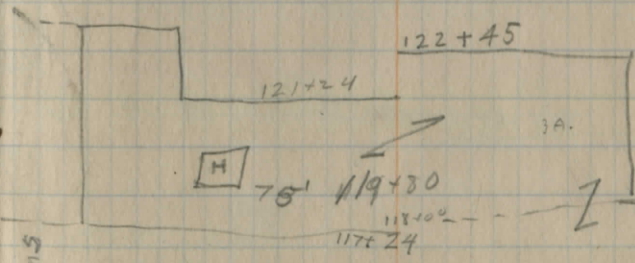
3/4 124+32

123+63

TWP

Bench

Abn Adams 123+10 80' [H]



[H] 100' 114+70

M. Stevens

110+50

A.K. Brown [H] 75' 108+30

Put culvert 108+05

PL 107+12

M. Stevens

PL 105+96 PL

Stage

C. Leggett

G. Garrett



13465

134+89

133+56



80

133705

132+63

80'



Belle Vernon Co

A. Little



80'

132+00

131+70

134+00

G. Garrett

Apron

131+12

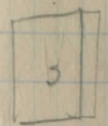
50

131+70



J. Walters

Alford & Stetson



40'

134+75

60'



Baldwin

F. Coe



80'

129+10

128+90

127+96

100'



Bench

143+53

PL 140+64

[D] 50' 140+40

[H] 50' 137+70

Mrs. M. Reden

250' [H]

PL 139+18

(W.A. Shaw?)

141+54

M. Alford
son J. Marey

[H] 200' 136+50

135+94

140+85 50' [ch]

Dis. Ch.

Mrs. L. Johnson

[H] 50' 135+70

140+37 PL

134+79

W. Emminger

138+50 ← 100' [H]

H. P. Whitney

[H]

137+35

PL

H. Alford

133+91 PL

137+06 75 [H]

Alford & Stetson

136+52 PL

[H]

[B. Fact.]

[H] 125 135+50

RL

154+20

F. Wolf

[H]

100 157+70

RL 157+73

stamm

[H]

75' 149+25

147+92

Cem-

143+38

144+92 RL

Cegielski
(W. Wolf Long)

[H]

60' 142+24

144+05 60'

[H]

M.E.ich

I. Clark

C. Roberts

P.L. 186+66⁵ P.L.

J. E. Phillips



170+70

176+80 60'

P.L.

173+15

173+57 P.L.

C. P. Nickom

J. Watters

172+30 60'

~~P.L.~~ P.L. 170+91

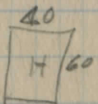
168+76 P.L.

A. Matur

J. Parlyshyn

60' 162+60

159+70



P.L. 159+24 P.L.

C. Roberts

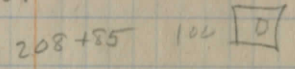
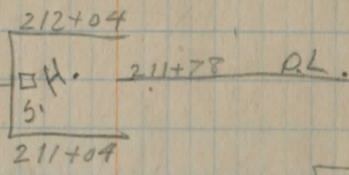
J. Peters

157+00 80'

213+60 RL

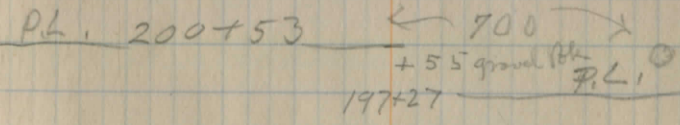
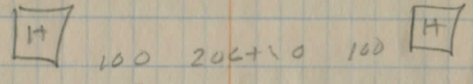
Jadkovick
35A
50

T. Hoffmay



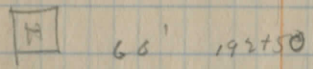
See

D. Velthuisen



J. M. Bradley

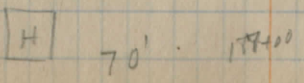
G. S. Hart



Road 192

G. S. Hart

B. Hart



B. Hart

251+60 PL₁

Jackson

146+40 125

H.

240+70 - Approx PL₁

Sidley

PL₁ 243+44

Joe Dolejs

H. 80' 238+40

J. N. Chaffee
Jackson

E. Rd

H. 100' 128+30

Webster

PL₁ 225+77 PL

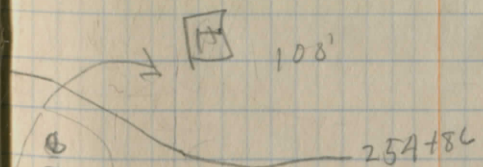
Webster

H. 80' 217+30

216+50 70' B

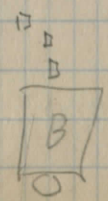
Hoffman

End



J.D. Vaxone

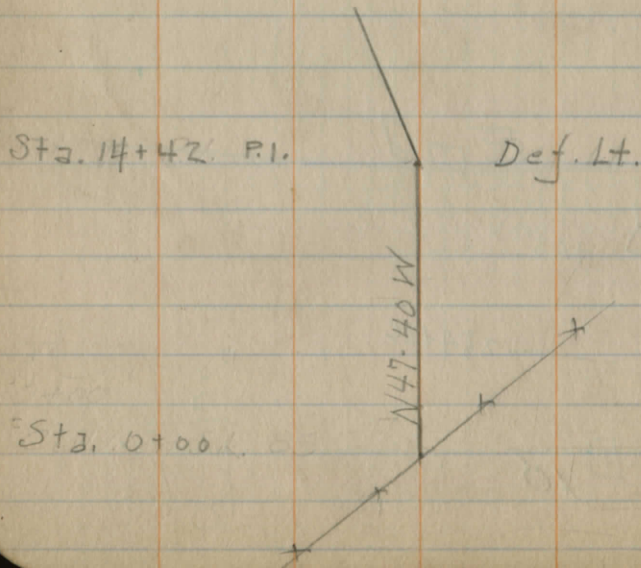
$253+75$
 $253+20$



Sidney

Montville Ditch Location Extension No 2

Stake out 154 ft. 1st. Ditch



Note Sta 14+42 = End of First Extension

1/12/34

Goodrich
Pomeroy
Richey

59

Levels Mentville Ditch Extension

No. 2

TWIN

BM[#] 10 0.70 1115.87 1115.17

Flow Stake 8.3 07.6

" stump. 3.45 1112.99 6.33 1109.54

2.95 1109.80 6.14 1106.85

BM[#] 11 6.89 1111.72 4.97 1104.83

Flow Stake 10.0 01.7

100 beyond 0+00 9.9

200 10.4

300 10.9

210 200 ft. 10.8 00.9

500 11.5

Elev.
Grade Rod at Stake

cut

Grades to Top of sidestakes

0+00 1111.72 10.55 1101.17 6.05

1 10.30 1101.42 5.40

2 10.05 1101.67 5.35

3 9.80 1101.92 5.20

4.43 1110.35 5.80 1105.92

4 8.18 1102.17 4.98

5 7.93 1102.42 4.43

Spike N. root Ash 100' E of Sta 16+00

Spike SW root 8" Elm 20' NE Sta 17+05

Notes: sidestakes numbered from
downstream end toward source

Sta 0+00 1101.17

0.25%

C 4.5

C 4.7

C 4.7 4.9

C 4.0

C 4.2

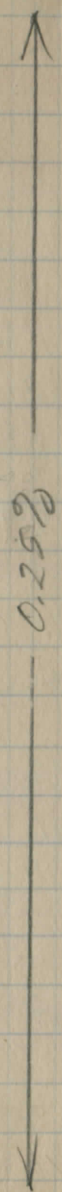
C 3.5

12
1.8
2.6

Grade Rod at Stake Cut

1110.35

Station	Grade	Rod at Stake	Cut
6	7.68	1102.67	3.62 C 4.0
7	7.43	1102.92	2.93 C 4.5 4'6"
8	7.18	1103.17	2.68 C 4.50 4'6"
9	6.93	1103.42	2.43 C 4.5 4'6"
10	5.84 1113.76 2.43	1107.92	5.59 C 4.50 4'6"
11	9.89	1103.92	3.84 C 6.0
12	9.59	1104.17	3.79 C 5.80 5'9 1/2"
13	9.34	1104.42	3.34 C 6.0
14	9.09	1104.67	2.99 C 6.80 6'9 1/2"
BM #10	7.83 1119.30 2.29	1111.47	
15	4.17	1115.13	1115.17
		1104.92	
16		1105.17	



BM Check Levels

BM # 10	4.17	1119.34		1115.17
TIP	4.27	1118.12	5.49	1113.85
	2.90	1119.93	1.09	1117.03
BM # 9			4.43	1115.50
	Bench Levels. STA 85 South east			
BM # 5	0.88	1125.65		1124.77
BM # 6	4.75	1125.65	4.75	1120.90
Flow Sta 58 Culvert			10.2	1114.4
	3.64	1123.47	5.82	1119.83
BM # 7	4.13	1123.47	4.13	1119.34
Flow Sta 53			8.4	115.1
Flow Sta 51			7.6	115.9
49	1.72	1122.69	2.50	1120.97
Flow Sta 46			8.8	113.9
	4.72	1124.65	2.76	1119.93
BM # 8	3.44	1124.65	3.44	1121.21
Flow Sta 41			11.1	113.5
38	4.35	1123.59	6.01	1118.64
Flow Sta 36			11.1	112.5
	3.53	1120.32	6.50	1116.79
Flow Sta 31			8.7	116
BM # 9			4.82	1115.50

Spike in NE root 24" Maple 60' Lt. of 29+75

S root 12" Maple N side State Rd 400' W of Sta 59+30 ✓

X cut SW 1/4 S Headwall Sta 59+05 ✓

Spike N root 8" Maple 175' SW Sta. 51

Spike NE root 24" Maple 40' SW Sta 40+30

1/16/33

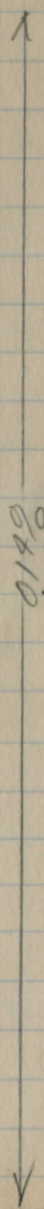
Goodrich
Pamerey
Richey

57

Grades to top of sidestakes		Grade	rod	cut	channel	
BM#10	335	1118.52	1115.17			
15		13.60	1104.92	7.10	C6.5	0.25%
16		13.35	1105.17	6.95	C6.5	10.1 3.2 Sta 16+00 X 1105.17
17		12.92	1105.60	6.92	C6.0	
18		12.50	1106.02	6.00	C6.5	Note: sidestakes numbered from downstream end toward source
	521	1117.73	6.00	1112.52		
19		11.28	1106.45	2.29	C9.0	
20		10.86	1106.87	4.86	C6.0	
21		10.43	1107.30	4.43	C6.0	0.425%
22		10.01	1107.72	4.51	C5.5	
23		9.59	1108.15	3.59	C6.0	
	742	1121.58	3.57	1114.16		
24		13.01	1108.57	7.01	C6.0	
25		12.58	1109.00	7.08	C5.5	10.8 18 Sta 25+00 X 1109.00
26		12.44	1109.14	5.99	C6.45	0.14%

Grade Rod Cut Channel

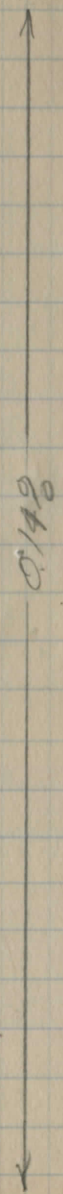
	1121.58						
27		12.30	1109.28	5.30	C 7.0		
28		12.16	1109.42	4.66	C 7.5		
	3.10 1120.02	4.66	1116.92				
29		10.46	1109.56	3.46	C 7.0		
34 = 90	4.56 1120.06	4.56	1115.46	1115.50			
30		10.36	1109.70	3.36	C 7.0		
31		10.22	1109.84	3.72	C 6.5	11.6	1.8
32		10.08	1109.98	3.58	C 6.5		
33		9.94	1110.12	2.74	C 7.0		
	6.47 1123.58	2.95	1117.11				
34		13.32	1110.26	6.82	C 6.5		
35		13.18	1110.40	5.68	C 7.5		
36		13.04	1110.54	5.54	C 7.5	12.5	2.0
37		12.90	1110.68	6.70	C 6.0		
38		12.76	1110.82	5.26	C 7.5		
	5.52 1123.84	5.26	1118.32				



Grade Rod Cut Channel

112384

			Grade	Rod	Cut	Channel	
39			12.88	111096	5.38	C 7.5	
40			12.74	1111.10	2.24	C 10.5	
BM ⁸			2.63	112421	1121.21		
41			12.60	1111.24	3.60	C 9.0	13.5 2.3
42			12.46	1111.38	4.96	C 7.5	
43			12.32	1111.52	4.32	C 5.0	
	306	112259	4.31	111253			
44			10.93	1111.66	2.93	C 8.0	
45			10.79	1111.80	3.29	C 7.5	
46			10.65	1111.94	3.65	C 7.0	13.2 2.0
47			10.51	1112.08	3.51	C 7.0	
48			10.37	1112.22	2.37	C 8.0	
	476	112429	2.36	112023			
49			12.63	1112.36	4.13	C 8.5	
50			12.49	1112.50	3.99	C 8.5	



	112499	Grade	Rod	Cut	Channel
BM#7		56.5 1119.34	1119.34		
51		12.35 1112.64	435	C 8.0	15.9 3.3
52		12.21 1112.78	571	C 6.5	
53		12.07 1112.92	507	C 7.0	15.1 2.2
	314 112307	506 1119.93			
54		10.03 1113.04	253	C 7.5	
55		9.89 1113.18	232	C 7.5	
56		9.75 1113.32	325	C 6.5	
57		9.61 1113.46	311	C 6.5	
58		7.47 1113.60	297	C 6.5	14.4 0.8
BM#6		216 1120.91	1120.90		

0.4%

Flow at culvert
 X cut SW of Headwall Sta 59+05 or
 S side of State R. 85 =
 (= U.S. # 6 0049-12-42)

Note: sta 59+05 = sta 29+87 of
 original improvement

BM #9 3.19 1118.69 1115.50
25 Grade 9.69 0900
Flow 25 7.9 108
4.78 1119.57 3.90 1114.79
Grade 21 12.27 0730
Flow 21 9.8 .8
5.82 1118.59 6.80 1112.77
BM #10 3.35 1115.24 1115.17
3.35 1118.52

1/16/33

Levels W. Lateral to top side stakes

BM #7	432	1123.66	1119.34	1112.64 Grade
1	2.35	1121.31	1113.14	
2	4.00	1119.66	1113.64	
3	3.54	1120.12	1114.14	
4	2.09	1121.57	1114.64	
5	1.68	1121.98	1115.14	
6	1.86	1121.80	1115.64	
Flow 6	7.5	1116.2		
100' up lateral 2	6.0			

Goodrich
Fleming
Richey

62

Sta 0 = Sta 61 of E Lateral

cut. C 7.17 7'2"

C 6.02 6'0"

C 5.78 6'0"

C 6.93 6'11"

C 6.84 6'10"

C 6.16 6'2"

95.00

B.M.	1.53	101.53		100.00
			1.51	100.00
			4.4	97.1
			5.8	95.7
T.P.	1.13	91.44	11.22	90.31
			7.2	84.2
			8.3	83.1
			10.4	81.0
			6.9	84.5
			7.7	83.7
			4.0	87.4
			3.9	87.5
			2.4	89.0
			8.0	91.0
			+ 2.1	top 6 "ov8" out let
				97.9

Note: Pins to
 be marked west
 (see sheet in file) to
 make straight line
 A-B

Most Sly cor. conc of West M.H.

" " " " E "
 ground at NW & new parcel
 " " NE " " "

ground SE pin

F/L SE &

F/L ± 100 downstream

ground SW pin

" " cor

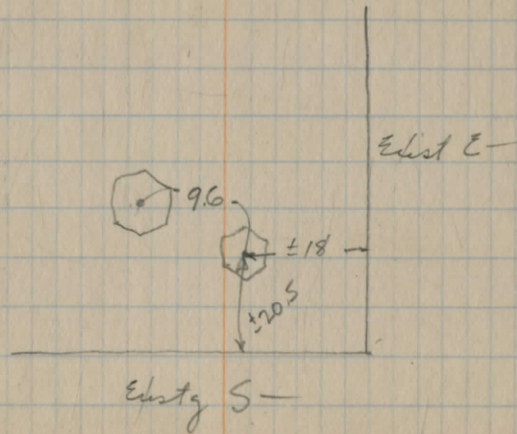
50' N of pin on W —

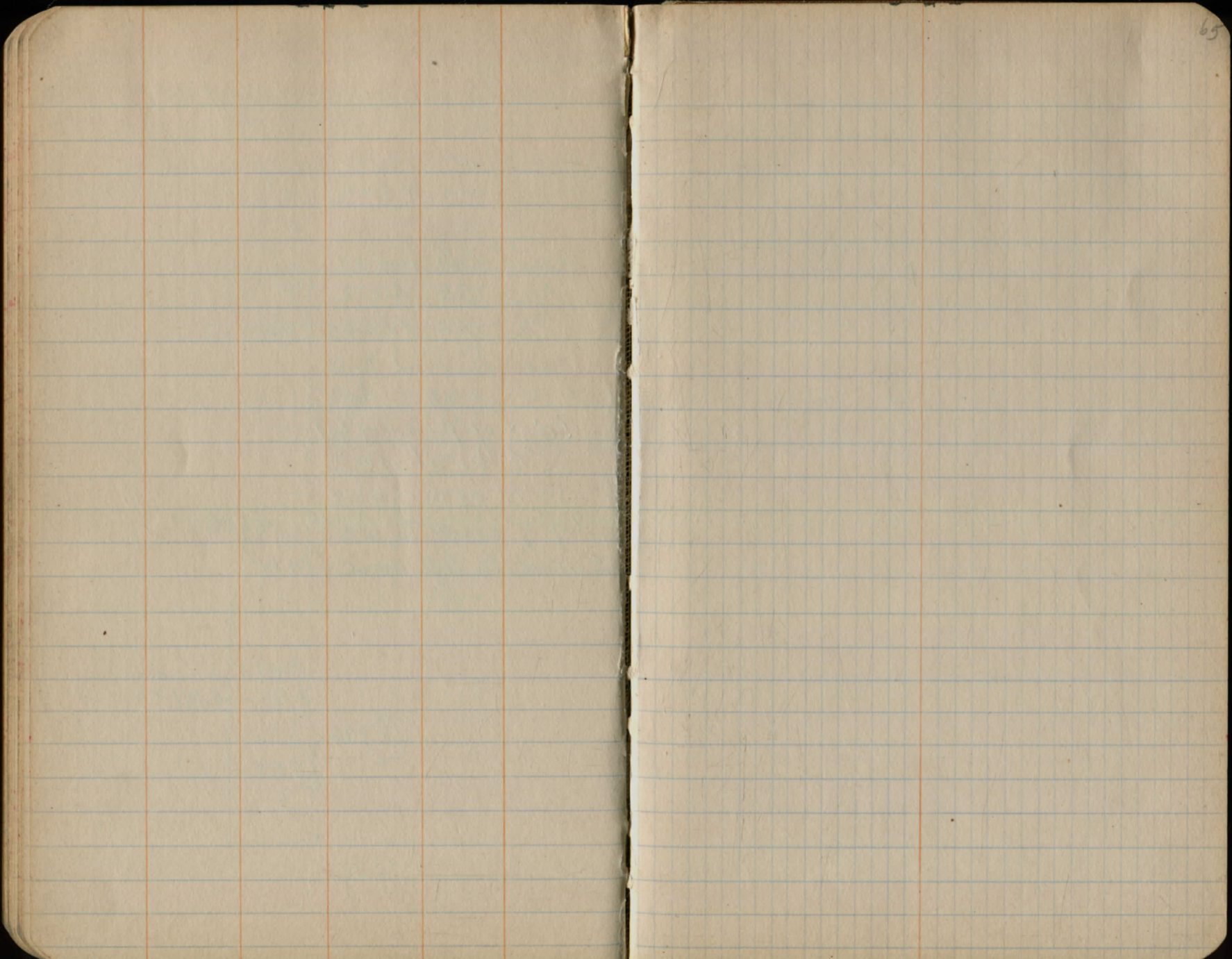
25' E of above

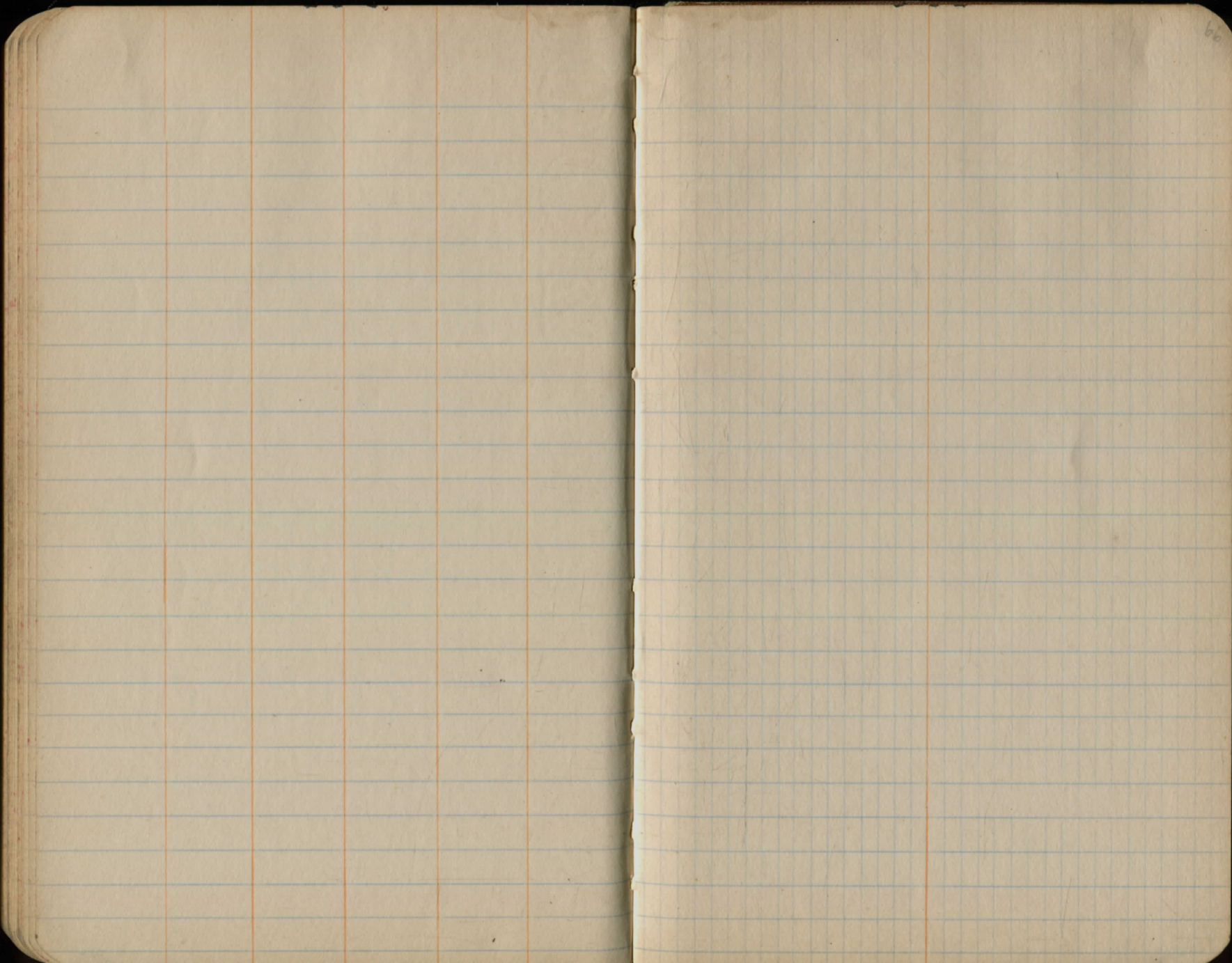
50' N of pin on E —

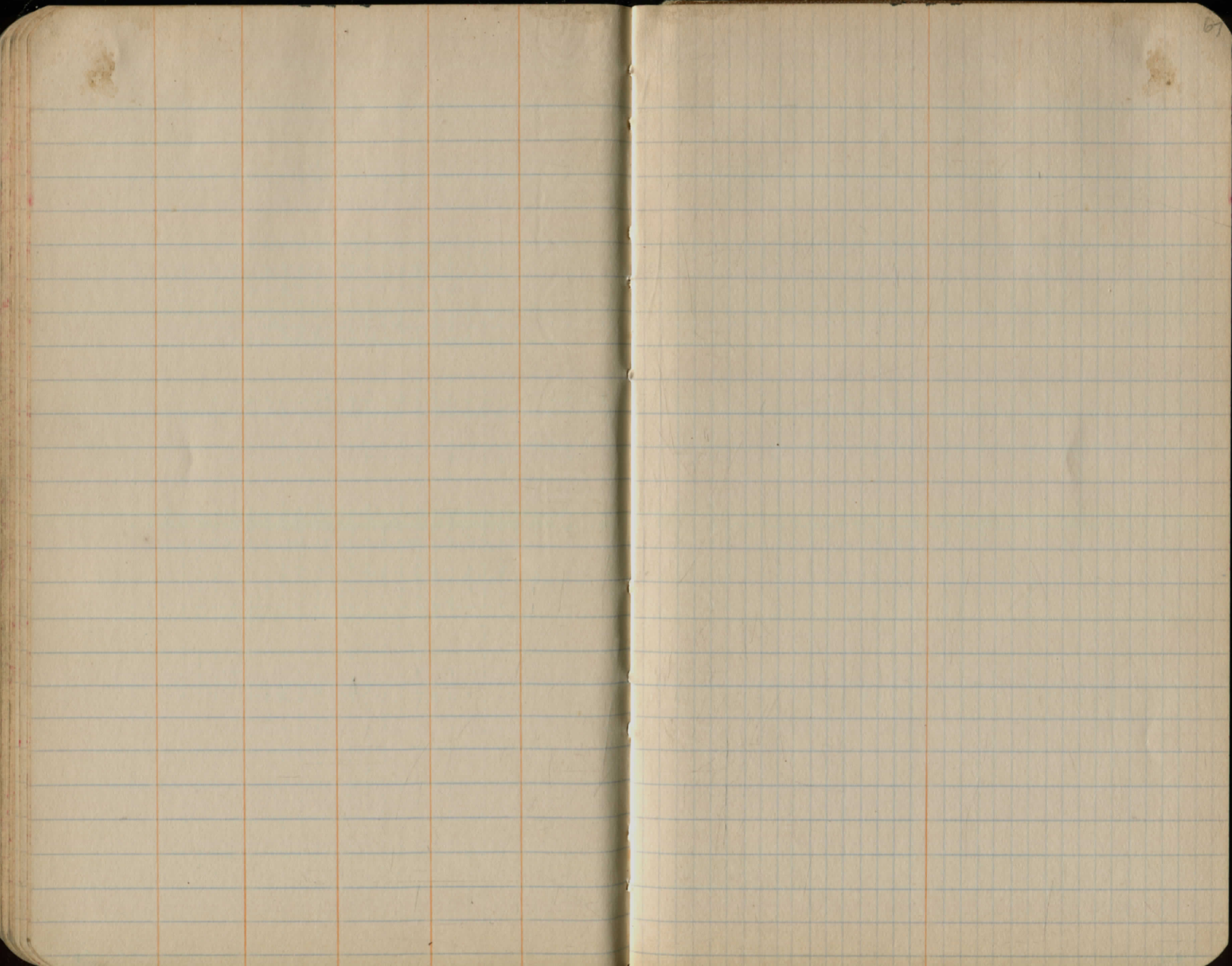
top of conc to bottom septee

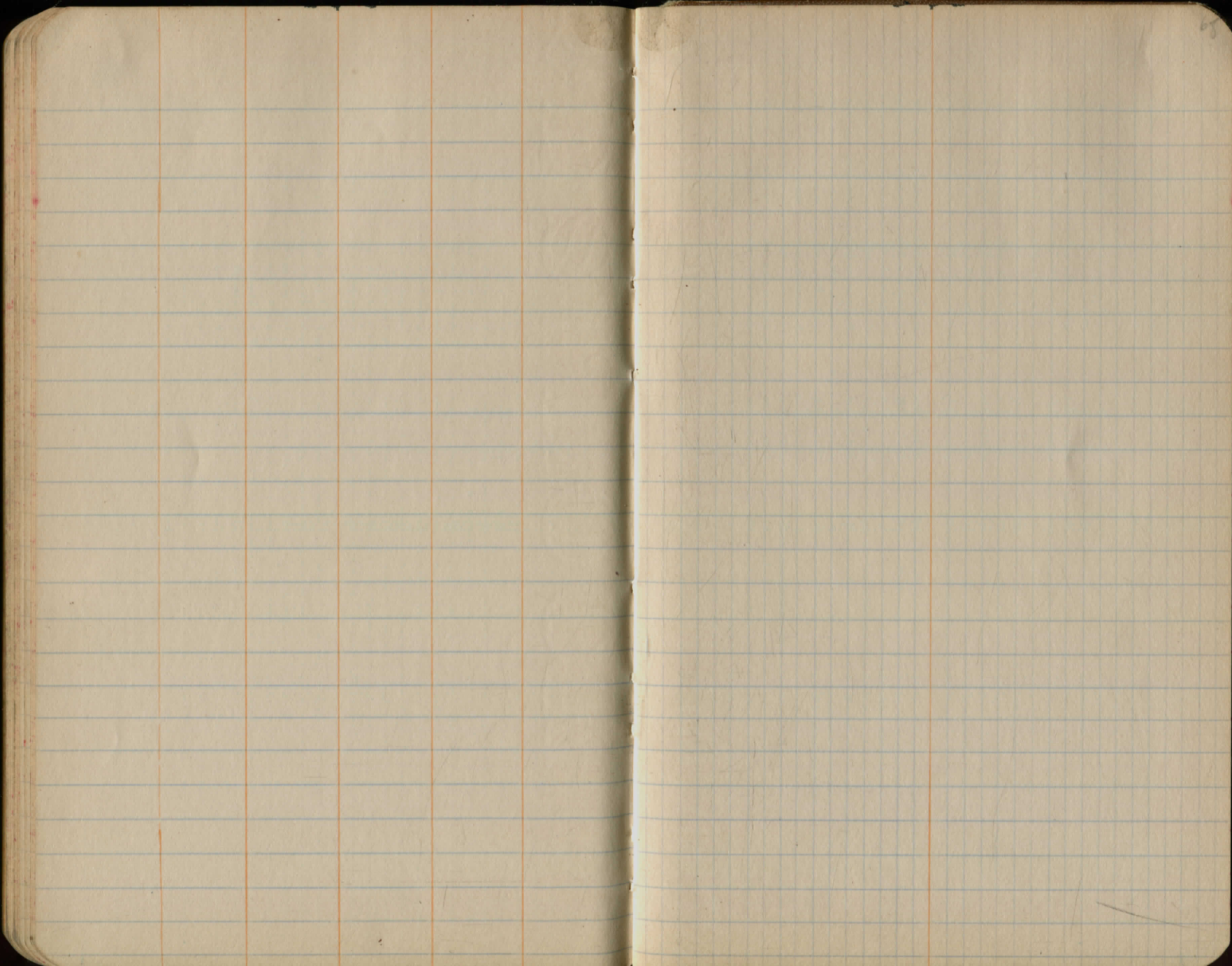
E M.H. to top conc M.H.

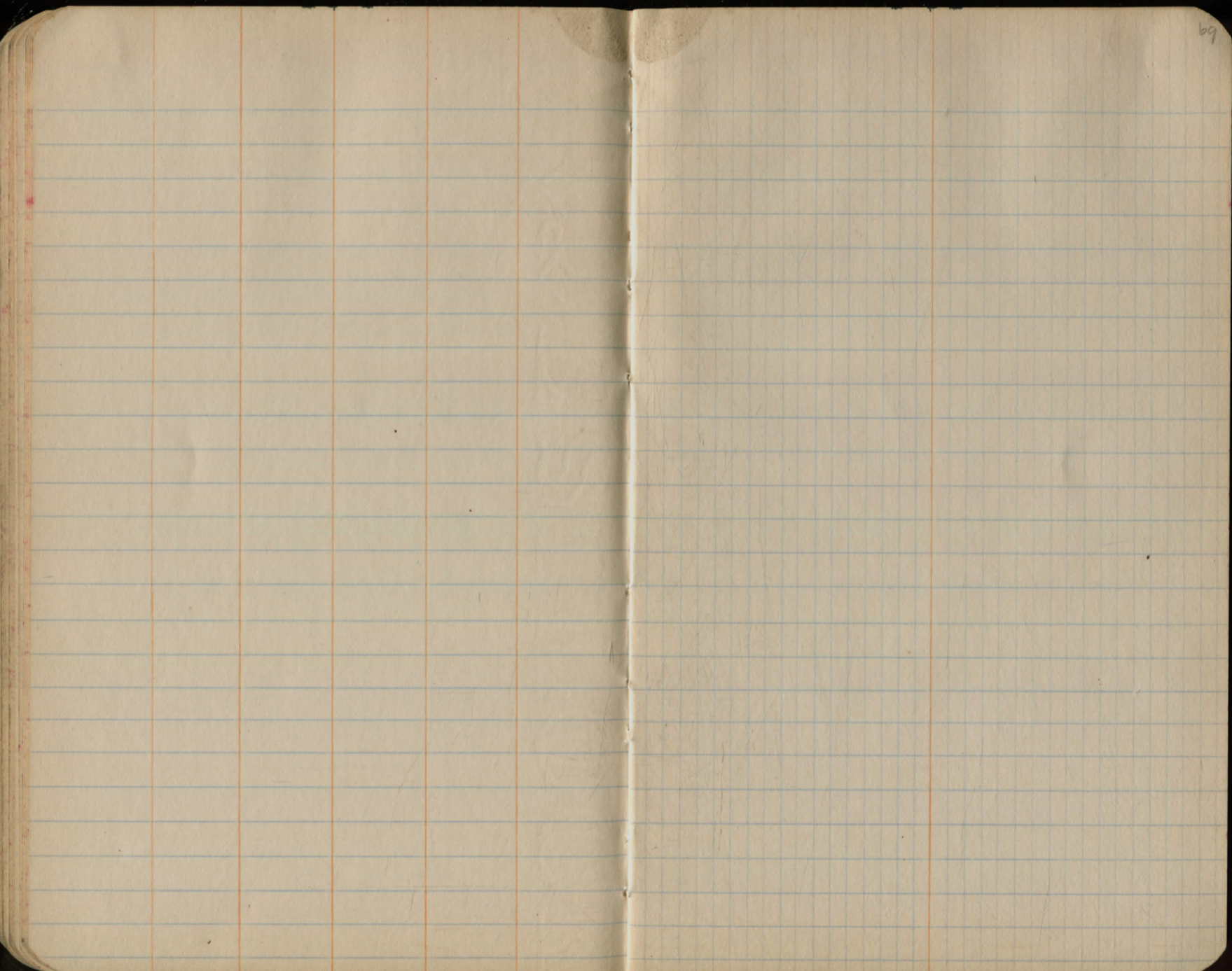


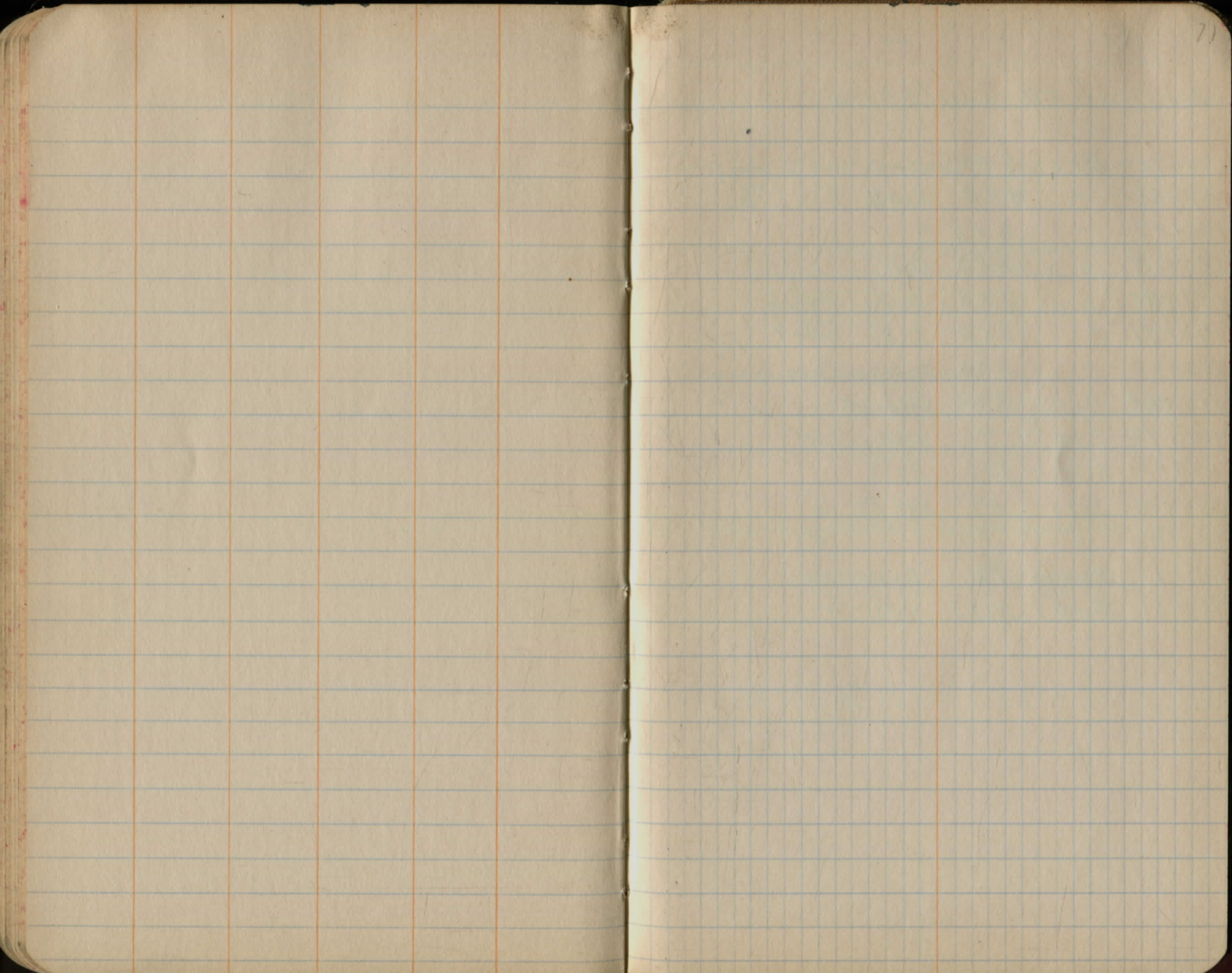












Offset stakes 20'-E - ROADWAY 20'

130+186 = E + W Center Rd

134+70 = Box 3 X 3 .

169+34 = " 4 X 3 EXT. EXT. 6'

174+97 " 2 X 2 P

185+69 " 2 X 3 O.K.

188+90 " 3 X 3 O.K. outlet

193+47 " 3 X 2 O.K. outlet

202+06 " 3 X 3 Relay ENDS Conc.

213+28 " 2 X 2 CLEAN OUT

219+92 Pipe ? OPEN OUTLET

227+31 BRIDGE 12 1/2' FAIR

234+00 PIPE 24" EXT. RT. 6'

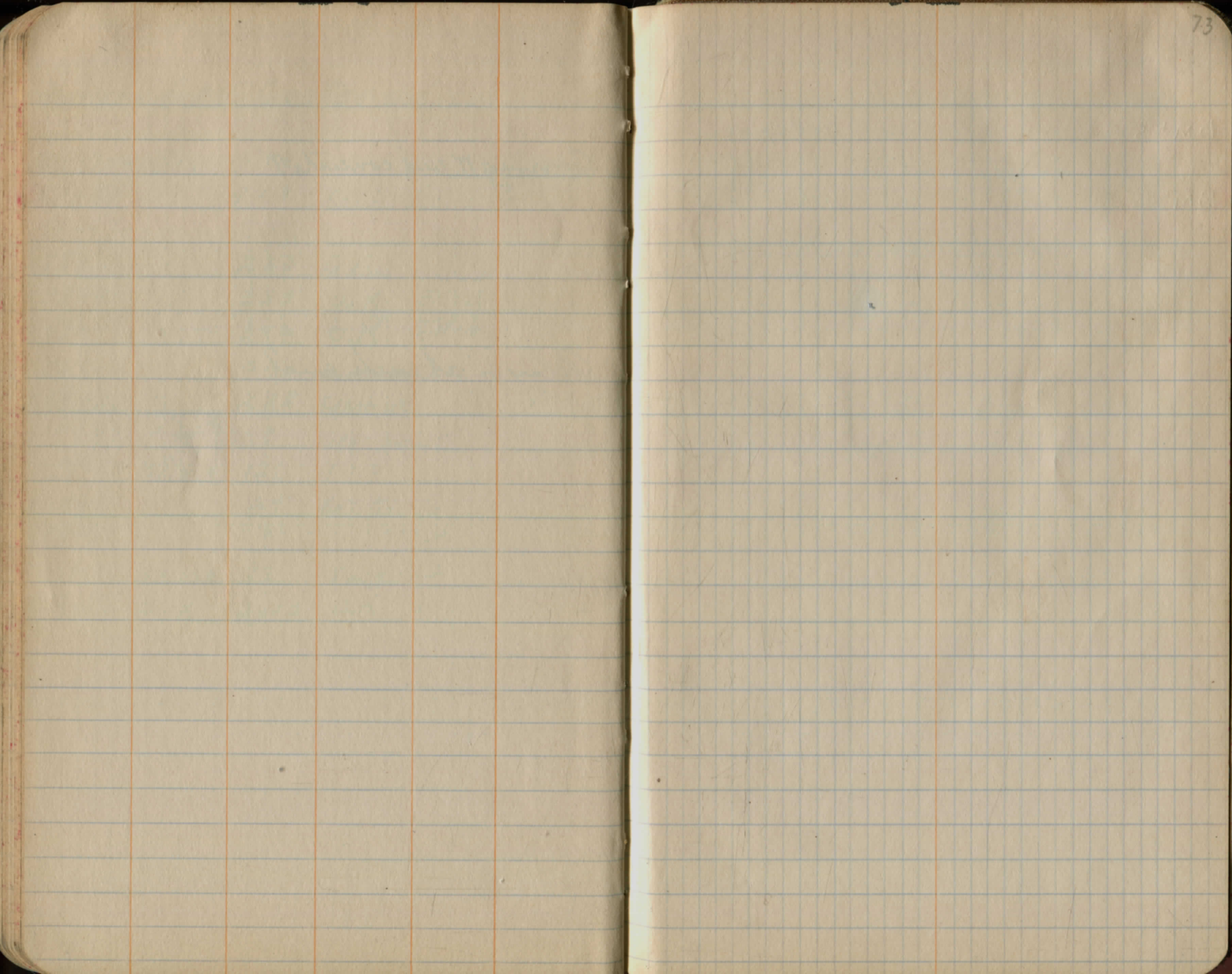
234+61 " ? ✓

245+00 BRIDGE 9 1/2' FAIR ✓

254+87 BOX 2 1/2 X 3 O.K. ✓

Covering W. end concrete 7'

Relay 6' at each end



BM[#]5

1124.77

BM[#]4

1126.76

74
Sroot 11" from trunk Maple left

54+75 - Ditch = 58+72

SW root 12" Maple 48+45

Prop Line = 49+59

U.S.G.S. B.M., Aluminum tablet
stamped "Cleveland 1239", set
in S.W. Cor. M.E. Church.
Elev. = 1238.286

INSTRUCTIONS FOR USE OF TABLES

TABLE No. 1.

Distance of slope stake from side or shoulder
Stake for any width roadway slope 1% to 1%
If ground is nearly level, the cut or fill at side

IMPROVED TABLES

AND

INFORMATION

TABLE No. 2.

To find Tangent and External for curve of
any other degree divide by degree of arc and
add correction found in column of corrections.

Degree of curve with a given L may be found
by dividing tangent (or external), opposite L by
given tangent (or external).

The distance from a point on the tangent to
the curve is very nearly the square of the tangent
length divided by twice the radius.

TABLE II—Continued
TRIGONOMETRIC FORMULAE (continued)

In any triangle:

Given a, b, C; to find c, B, A.

Use Law of Lines.

Given A, B, c; to find a, b, C.

Use Law of Lines.

Given a, b, c; to find A, B, C.

$$\text{Let } \frac{a+b+c}{2} = s, \sqrt{\frac{(s-a)(s-b)(s-c)}{s}} = r$$

$$\cos \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$$

$$\tan \frac{1}{2} A = \frac{r}{s-a}$$

$$\tan \frac{1}{2} B = \frac{r}{s-b}$$

$$\tan \frac{1}{2} C = \frac{r}{s-c}$$

Area of a triangle:

$$\text{Area} = \frac{1}{2} ab \sin C$$

$$\text{Area} = \sqrt{s(s-a)(s-b)(s-c)}$$

PRISMOIDAL FORMULA

$$\text{Vol.} = \frac{h}{6} (B+b+4M)$$

h = altitude; b, B = bases; M = midsection

TABLE III
INCHES AND FRACTIONS OF AN INCH IN DECIMALS OF A FOOT

	0	1	2	3	4	5	6	7	8	9	10	11
$\frac{1}{16}$.0052	.0885	.1719	.2552	.3385	.4219	.5052	.5885	.6719	.7552	.8385	.9219
$\frac{1}{8}$.0104	.0938	.1771	.2604	.3438	.4271	.5104	.5938	.6771	.7604	.8438	.9271
$\frac{3}{16}$.0156	.0990	.1823	.2656	.3490	.4323	.5156	.5990	.6823	.7656	.8490	.9323
$\frac{1}{4}$.0208	.1042	.1875	.2708	.3542	.4375	.5208	.6042	.6875	.7708	.8542	.9375
$\frac{5}{16}$.0260	.1094	.1927	.2760	.3594	.4427	.5260	.6094	.6927	.7760	.8594	.9427
$\frac{3}{8}$.0313	.1146	.1979	.2813	.3646	.4479	.5313	.6146	.6979	.7813	.8646	.9479
$\frac{7}{16}$.0365	.1198	.2031	.2865	.3698	.4531	.5365	.6198	.7031	.7865	.8698	.9531
$\frac{1}{2}$.0417	.1250	.2083	.2917	.3750	.4583	.5417	.6250	.7083	.7917	.8750	.9583
$\frac{9}{16}$.0469	.1302	.2135	.2969	.3803	.4635	.5469	.6302	.7135	.7969	.8802	.9635
$\frac{5}{8}$.0521	.1354	.2188	.3021	.3854	.4688	.5521	.6354	.7188	.8021	.8854	.9688
$\frac{11}{16}$.0573	.1406	.2240	.3073	.3906	.4740	.5573	.6406	.7240	.8073	.8906	.9740
$\frac{3}{4}$.0625	.1458	.2292	.3125	.3958	.4792	.5625	.6458	.7292	.8125	.8958	.9792
$\frac{13}{16}$.0677	.1510	.2344	.3177	.4010	.4844	.5677	.6510	.7344	.8177	.9010	.9844
$\frac{7}{8}$.0729	.1563	.2396	.3229	.4063	.4896	.5729	.6563	.7396	.8229	.9063	.9896
$\frac{15}{16}$.0781	.1615	.2448	.3281	.4115	.4948	.5781	.6615	.7448	.8281	.9115	.9948
1	.0833	.1667	.2500	.3333	.4167	.5000	.5833	.6667	.7500	.8333	.9167	1.0000
	0	1	2	3	4	5	6	7	8	9	10	11

TABLE IV
USEFUL RELATIONS.

Lineal feet	×.00019	= miles
Lineal yards	×.0006	= miles
Square inches	×.007	= square feet
Square feet	×.111	= square yards
Square yards	×.0002067	= acres
Acres	×4840	= square yards
Cubic inches	×.00058	= cubic feet
Cubic feet	×.03704	= cubic yards
Links	×.22	= yards
Links	×.66	= feet
Feet	×1.5	= links

$$360^\circ = 21600' = 1296000''$$

$$\text{Radius} = \text{arc of } 57.2957790'$$

$$\text{Arc of } 1^\circ (\text{radius} = 1) = .017453292$$

$$\text{Arc of } 1' (\text{radius} = 1) = .000290888$$

$$\text{Arc of } 1'' (\text{radius} = 1) = .000004848$$

$$\pi = 3.141592654 \quad \sqrt{\frac{1}{4}} = 0.564190$$

$$\frac{\pi}{4} = 0.785398163 \quad \sqrt[3]{\frac{6}{\pi}} = 1.240700982$$

$$\frac{\pi}{6} = 0.523598776 \quad \pi^2 = 9.869604401$$

$$\sqrt{\frac{4}{\pi}} = 1.128379167 \quad \frac{1}{\pi^2} = 0.101321184$$

$$\frac{\pi}{6} = 0.523598776 \quad \sqrt{\pi} = 1.772453851$$

$$\frac{4\pi}{3} = 4.188790205 \quad \frac{1}{\pi} = 0.3183099$$

Curvature of Earth's surface = about 0.7 feet in 1 mile

Curvature in feet = $0.667 (\text{Dist. in miles})^2$

Difference between arc and chord length, 0.05 feet in $11\frac{1}{2}$ miles

$$\text{Probable error of a single observation} = 0.6754 \sqrt{\frac{M v^2}{n-1}}$$

Error in chaining of 0.01 feet in 100 feet:

Due to—

1. Length of tape error of 0.01 feet
2. Alignment. One end 1.4 feet out of line
3. Sag of tape at centre of 0.61 feet.
4. Temperature difference of 15°
5. Difference of pull of 15 lbs.

STADIA REDUCTION FORMULÆ.

$$\text{Horizontal Distance} = R - R \sin^2 a + C \cos a$$

$$\text{Vertical Distance} = R \frac{1}{2} \sin^2 a + C \sin a$$

$$R = \text{Reading} \times \frac{\text{distance from Object glass to cross hairs}}{\text{distance between cross hairs}}$$

C = distance from Object glass to cross hairs + distance from Object glass to center of instrument.

a = angle of elevation for mid Reading

TABLE VI (continued)
SINES, COSINES, TANGENTS, COTANGENTS (continued)

deg.	sin 0'	tan 0'	sin 10'	tan 10'	sin 20'	tan 20'	sin 30'	tan 30'	sin 40'	tan 40'	sin 50'	tan 50'	deg.
46	7193	1.0355	7214	1.0416	7234	1.0477	7254	1.0533	7274	1.0599	7294	1.0661	43
47	314	.0724	333	.0786	353	.0850	373	.0913	392	.0977	412	.1041	42
48	431	.1106	451	.1171	470	.1237	490	.1303	509	.1369	528	.1436	41
49	547	.1504	566	.1571	585	.1640	604	.1708	623	.1778	642	.1847	40
50	660	1.1918	7679	1.1988	7698	1.2059	7716	1.2131	7735	1.2203	7753	1.2276	39
51	771	2349	790	.2423	808	.2497	826	.2572	844	.2647	862	.2723	38
52	880	2709	898	.2876	916	.2954	934	.3032	951	.3111	969	.3190	37
53	986	3270	8004	.3351	8021	.3452	8039	.3514	8056	.3597	8073	.3680	36
54	8090	3764	107	.3848	124	.3934	141	.4019	158	.4106	175	.4193	35
55	192	4281	208	.4370	225	.4460	241	.4550	258	.4641	274	.4733	34
56	290	4826	307	.4919	323	.5013	339	.5108	355	.5204	371	.5301	33
57	387	5399	403	.5497	418	.5597	434	.5697	450	.5798	465	.5900	32
58	480	6003	496	.6107	511	.6212	526	.6319	542	.6426	557	.6534	31
59	572	6643	587	.6753	601	.6864	616	.6977	631	.7090	646	.7205	30
60	660	1.7321	8675	1.7437	8689	1.7556	8704	1.7675	8718	1.7797	8732	1.7917	29
61	746	.8040	760	.8165	774	.8291	788	.8418	802	.8546	816	.8676	28
62	829	8807	843	.8940	857	.9074	870	.9210	884	.9347	897	.9486	27
63	910	9626	923	.9768	936	.9912	949	2.0057	962	2.0204	975	2.0353	26
64	988	2.0503	9001	2.0655	9013	2.0809	9026	.0965	9038	.1123	9051	.1283	25
65	9063	1.445	075	.1609	088	.1775	100	.1943	112	.2113	124	.2286	24
66	135	.2460	147	.2637	159	.2817	171	.2998	182	.3183	194	.3369	23
67	205	3559	216	.3750	228	.3945	239	.4142	250	.4342	261	.4545	22
68	272	4751	283	.4960	293	.5172	304	.5386	315	.5605	325	.5826	21
69	336	6051	346	.6279	356	.6511	367	.6746	377	.6985	387	.7228	20
70	397	2.7475	9407	2.7725	9417	2.7980	9426	2.8239	9436	2.8502	9446	2.8770	19
71	455	.9042	465	.9319	474	.9600	483	.9887	492	3.0178	502	3.0475	18
72	511	3.0777	520	3.1084	528	3.1397	537	3.1716	546	.2041	555	.2371	17
73	563	2.709	572	.3052	580	.3402	588	.3759	596	.4124	605	.4495	16
74	613	4.874	621	.5261	628	.5656	636	.6059	644	.6470	652	.6891	15
75	659	7.321	667	.7760	674	.8208	681	.8657	689	.9136	696	.9617	14
76	703	4.0108	710	4.0611	717	4.1126	724	4.1653	730	4.2193	737	4.2743	13
77	744	.3315	750	.3897	757	.4494	763	.5107	769	.5736	775	.6382	12
78	781	.7046	787	.7729	793	.8430	799	.9152	805	.9894	811	5.0658	11
79	816	.1446	822	5.2257	827	5.3093	833	5.3955	838	5.4845	843	.5764	10
80	9848	5.6713	9853	5.7694	9858	5.8708	9863	5.9758	9868	6.0844	9872	6.1970	9
81	877	6.3138	881	6.4348	886	6.5606	890	6.6912	894	.8269	899	.9682	8
82	903	7.1154	907	7.2687	911	7.4287	914	7.5958	918	7.7704	922	7.9530	7
83	925	8.1443	929	8.3450	932	8.5555	936	8.7769	939	9.0098	942	9.2553	6
84	945	9.5144	948	9.7882	951	10.078	954	10.385	957	10.711	959	11.059	5
85	962	11.430	964	11.826	967	12.250	969	12.706	971	13.197	974	13.727	4
86	976	14.300	978	14.924	980	15.605	981	16.350	983	17.169	985	18.075	3
87	986	19.081	988	20.206	989	21.470	990	22.903	992	24.542	993	26.432	2
88	994	28.636	995	31.242	996	34.368	997	38.189	997	42.964	998	49.104	1
89	9998	57.290	9999	68.750	9999	85.940	9999	114.58	1.000	171.88	1.000	343.77	0
deg.	60'	60'	50'	50'	40'	40'	30'	30'	20'	30'	10'	10'	deg.
	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	cos	cot	

TABLE VII
RODS IN FEET AND INCHES

Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches	Rods	Feet Inches
1	16-6	21	346-6	41	676-6	61	1006-6	81	1336-6
2	33-0	22	363-0	42	693-0	62	1023-0	82	1353-0
3	49-6	23	379-6	43	709-6	63	1039-6	83	1369-6
4	66-0	24	396-0	44	726-0	64	1056-0	84	1386-0
5	82-6	25	412-6	45	742-6	65	1072-6	85	1402-6
6	99-0	26	429-0	46	759-0	66	1089-0	86	1419-0
7	115-6	27	445-6	47	775-6	67	1105-6	87	1435-6
8	132-0	28	462-0	48	792-0	68	1122-0	88	1452-0
9	148-6	29	478-6	49	808-6	69	1138-6	89	1468-6
10	165-0	30	495-0	50	825-0	70	1155-0	90	1485-0
11	181-6	31	511-6	51	841-6	71	1171-6	91	1501-6
12	198-0	32	528-0	52	858-0	72	1188-0	92	1518-0
13	214-6	33	544-6	53	874-6	73	1204-6	93	1534-6
14	231-0	34	561-0	54	891-0	74	1221-0	94	1551-0
15	247-6	35	577-6	55	907-6	75	1237-6	95	1567-6
16	264-0	36	594-0	56	924-0	76	1254-0	96	1584-0
17	280-6	37	610-6	57	940-6	77	1270-6	97	1600-6
18	297-0	38	627-0	58	957-0	78	1287-0	98	1617-0
19	313-6	39	643-6	59	973-6	79	1303-6	99	1633-6
20	330-0	40	660-0	60	990-0	80	1320-0	100	1650-0

TABLE VIII
LINKS IN FEET AND INCHES

Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches	Links	Feet Inches
1	0-7.92	18	11-10.56	35	23-1.20	52	34-3.84	69	45-6.48	86	56-9.12
2	1-3.84	19	12-6.48	36	23-9.12	53	34-11.76	70	46-2.40	87	57-5.04
3	1-11.76	20	13-2.40	37	24-5.04	54	35-7.68	71	46-10.32	88	58-0.96
4	2-7.68	21	13-10.32	38	25-0.96	55	36-3.60	72	47-6.24	89	58-8.88
5	3-3.60	22	14-6.24	39	25-8.88	56	36-11.52	73	48-2.16	90	59-4.80
6	3-11.52	23	15-2.16	40	26-4.80	57	37-7.44	74	48-10.08	91	60-0.72
7	4-7.44	24	15-10.08	41	27-0.72	58	38-3.36	75	49-6.00	92	60-8.64
8	5-3.36	25	16-6.00	42	27-8.64	59	38-11.28	76	50-1.92	93	61-4.56
9	5-11.28	26	17-1.92	43	28-4.56	60	39-7.20	77	50-9.84	94	62-0.48
10	6-7.20	27	17-9.84	44	29-0.48	61	40-3.12	78	51-5.76	95	62-8.40
11	7-3.12	28	18-5.76	45	29-8.40	62	40-11.04	79	52-1.68	96	63-4.32
12	7-11.04	29	19-1.68	46	30-4.32	63	41-6.96	80	52-9.60	97	64-0.24
13	8-6.96	30	19-9.60	47	31-0.24	64	42-2.88	81	53-5.52	98	64-8.16
14	9-2.88	31	20-5.52	48	31-8.16	65	42-10.80	82	54-1.44	99	65-4.08
15	9-10.80	32	21-1.44	49	32-4.08	66	43-6.72	83	54-9.36	100	66-0.00
16	10-6.72	33	21-9.36	50	33-0.00	67	44-2.64	84	55-5.28	101	66-7.92
17	11-2.64	34	22-5.28	51	33-7.92	68	44-10.56	85	56-1.20	102	67-3.84

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=10°	I	T	E	I=20°	I	T	E	I=30°
1°	50.00	218	+	11°	551.70	26.500	+	21°	1061.9	97.577	+
10'	58.34	.287	5° C.	10'	560.11	27.313	5° C.	10'	1070.6	99.155	5° C.
20'	66.67	.398	T	20'	568.53	28.137	T	20'	1079.2	100.775	T
30'	75.01	.491	.03	30'	576.95	28.974	.06	30'	1087.8	102.355	.10
40'	83.34	.606	E	40'	585.36	29.824	E	40'	1096.4	103.97	E
50'	91.68	.733	.001	50'	593.79	30.686	.006	50'	1105.1	105.60	.013
2°	100.01	.873	10° C.	12°	602.21	31.561	10° C.	22°	1113.7	107.24	10° C.
10'	108.35	1.024	T	10'	610.64	32.447	T	10'	1122.4	108.90	T
20'	116.68	1.188	.06	20'	619.07	33.347	.13	20'	1131.0	110.57	.19
30'	125.02	1.364	E	30'	627.50	34.259	E	30'	1139.7	112.25	E
40'	133.36	1.552	.003	40'	635.93	35.183	.011	40'	1148.4	113.95	.025
50'	141.70	1.752	15° C.	50'	644.37	36.120	15° C.	50'	1157.0	115.66	15° C.
3°	150.04	1.964	T	13°	652.81	37.070	T	23°	1165.7	117.38	T
10'	158.38	2.188	E	10'	661.25	38.031	E	10'	1174.4	119.12	E
20'	166.72	2.425	.06	20'	669.70	39.006	.13	20'	1183.1	120.87	.26
30'	175.06	2.674	E	30'	678.15	39.993	E	30'	1191.8	122.63	.40
40'	183.40	2.934	.003	40'	686.60	40.992	.011	40'	1200.5	124.41	.046
50'	191.74	3.207	15° C.	50'	695.06	42.004	15° C.	50'	1209.2	126.20	15° C.
4°	200.08	3.492	T	14°	703.51	43.029	T	24°	1217.9	128.00	T
10'	208.43	3.790	E	10'	711.97	44.066	E	10'	1226.6	129.82	E
20'	216.77	4.099	.06	20'	720.44	45.116	.13	20'	1235.3	131.65	.26
30'	225.12	4.421	E	30'	728.90	46.178	E	30'	1244.0	133.50	.40
40'	233.47	4.755	.003	40'	737.37	47.253	.011	40'	1252.8	135.35	.046
50'	241.81	5.100	15° C.	50'	745.85	48.341	15° C.	50'	1261.5	137.23	15° C.
5°	250.16	5.459	T	15°	754.32	49.441	T	25°	1270.2	139.11	T
10'	258.51	5.829	E	10'	762.80	50.554	E	10'	1279.0	141.01	E
20'	266.86	6.211	.06	20'	771.29	51.679	.13	20'	1287.7	142.93	.26
30'	275.21	6.606	E	30'	779.77	52.818	E	30'	1296.5	144.85	.40
40'	283.57	7.013	.003	40'	788.26	53.969	.011	40'	1305.3	146.79	.046
50'	291.92	7.432	15° C.	50'	796.75	55.132	15° C.	50'	1314.0	148.75	15° C.
6°	300.28	7.863	T	16°	805.25	56.309	T	26°	1322.8	150.71	T
10'	308.64	8.307	E	10'	813.75	57.498	E	10'	1331.6	152.69	E
20'	316.99	8.762	.06	20'	822.25	58.699	.13	20'	1340.4	154.69	.26
30'	325.35	9.230	E	30'	830.76	59.914	E	30'	1349.2	156.70	.40
40'	333.71	9.710	.003	40'	839.27	61.141	.011	40'	1358.0	158.72	.046
50'	342.08	10.202	15° C.	50'	847.78	62.381	15° C.	50'	1366.8	160.76	15° C.
7°	350.44	10.707	T	17°	856.30	63.634	T	27°	1375.6	162.81	T
10'	358.81	11.224	E	10'	864.82	64.900	E	10'	1384.4	164.86	E
20'	367.17	11.753	.06	20'	873.35	66.178	.13	20'	1393.2	166.95	.26
30'	375.54	12.294	E	30'	881.88	67.470	E	30'	1402.0	169.04	.40
40'	383.91	12.847	.003	40'	890.41	68.774	.011	40'	1410.9	171.15	.046
50'	392.28	13.413	15° C.	50'	898.95	70.091	15° C.	50'	1419.7	173.27	15° C.
8°	400.66	13.991	T	18°	907.49	71.421	T	28°	1428.6	175.41	T
10'	409.03	14.582	E	10'	916.03	72.764	E	10'	1437.4	177.55	E
20'	417.41	15.184	.06	20'	924.58	74.119	.13	20'	1446.3	179.72	.26
30'	425.79	15.799	E	30'	933.13	75.488	E	30'	1455.1	181.89	.40
40'	434.17	16.426	.003	40'	941.69	76.869	.011	40'	1464.0	184.08	.046
50'	442.55	17.065	15° C.	50'	950.25	78.264	15° C.	50'	1472.9	186.29	15° C.
9°	450.93	17.717	T	19°	958.81	79.671	T	29°	1481.8	188.51	T
10'	459.32	18.381	E	10'	967.38	81.092	E	10'	1490.7	190.74	E
20'	467.71	19.058	.06	20'	975.96	82.525	.13	20'	1499.6	192.99	.26
30'	476.10	19.746	E	30'	984.53	83.972	E	30'	1508.5	195.25	.40
40'	484.49	20.447	.003	40'	993.12	85.431	.011	40'	1517.4	197.53	.046
50'	492.88	21.161	15° C.	50'	1001.7	86.904	15° C.	50'	1526.3	199.82	15° C.
10°	501.28	21.887	T	20°	1010.3	88.389	T	30°	1535.3	202.12	T
10'	509.68	22.624	E	10'	1018.9	89.888	E	10'	1544.2	204.44	E
20'	518.08	23.375	.06	20'	1027.5	91.399	.13	20'	1553.1	206.77	.26
30'	526.48	24.138	E	30'	1036.1	92.924	E	30'	1562.1	209.12	.40
40'	534.89	24.913	.003	40'	1044.7	94.462	.011	40'	1571.0	211.48	.046
50'	543.29	25.700	15° C.	50'	1053.3	96.013	.034	50'	1580.0	213.86	.078

T = R tan 1/2 I

E = R exsec 1/2 I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=40°	I	T	E	I=50°	I	T	E	I=60°
31°	1589.0	216.3	+	41°	2142.2	387.4	+	51°	2732.9	618.4	+
10'	1598.0	218.7	5° C.	10'	2151.7	390.7	5° C.	10'	2743.1	622.8	5° C.
20'	1606.9	221.1	T	20'	2161.2	394.1	T	20'	2753.4	627.2	T
30'	1615.9	223.5	.13	30'	2170.8	397.4	.17	30'	2763.7	631.7	.21
40'	1624.9	226.0	E	40'	2180.3	400.8	E	40'	2773.9	636.2	E
50'	1633.9	228.4	.023	50'	2189.9	404.2	.037	50'	2784.2	640.7	.056
32°	1643.0	230.9	10° C.	42°	2199.4	407.6	10° C.	52°	2794.5	645.2	10° C.
10'	1652.0	233.4	T	10'	2209.0	411.1	T	10'	2804.9	649.7	T
20'	1661.0	235.9	.06	20'	2218.6	414.5	.10	20'	2815.2	654.3	.14
30'	1670.0	238.4	E	30'	2228.1	418.0	E	30'	2825.6	658.8	E
40'	1679.1	241.0	.013	40'	2237.7	421.4	.017	40'	2835.9	663.4	.021
50'	1688.1	243.5	15° C.	50'	2247.3	425.0	15° C.	50'	2846.3	668.0	15° C.
33°	1697.2	246.1	T	43°	2257.0	428.5	T	53°	2856.7	672.7	T
10'	1706.3	248.7	E	10'	2266.6	432.0	E	10'	2867.1	677.3	E
20'	1715.3	251.3	.06	20'	2276.2	435.6	.10	20'	2877.5	682.0	.14
30'	1724.4	253.9	E	30'	2285.9	439.2	E	30'	2888.0	686.7	E
40'	1733.5	256.5	.013	40'	2295.6	442.8	.017	40'	2898.4	691.4	.017
50'	1742.6	259.1	15° C.	50'	2305.2	446.4	.021	50'	2908.9	696.1	.021
34°	1751.7	261.8	T	44°	2314.9	450.0	T	54°	2919.4	700.9	T
10'	1760.8	264.5	E	10'	2324.6	453.6	E	10'	2929.9	705.7	E
20'	1770.0	267.2	.06	20'	2334.3	457.3	.10	20'	2940.4	710.5	.14
30'	1779.1	269.9	E	30'	2344.1	461.0	E	30'	2951.0	715.3	E
40'	1788.2	272.6	.013	40'	2353.8	464.6	.017	40'	2961.5	720.1	.017
50'	1797.4	275.3	15° C.	50'	2363.5	468.4	15° C.	50'	2972.1	725.0	15° C.
35°	1806.6	278.1	T	45°	2373.3	472.1	T	55°	2982.7	729.9	T
10'	1815.7	280.8	E	10'	2383.1	475.8	E	10'	2993.3	734.8	E
20'	1824.9	283.6	.06	20'	2392.8	479.6	.10	20'	3003.9	739.7	.14
30'	1834.1	286.4	E	30'	2402.6	483.4	E	30'	3014.5	744.6	E
40'	1843.3	289.2	.013	40'	2412.4	487.2	.017	40'	3025.2	749.6	.017
50'	1852.5	292.0	15° C.	50'	2422.3	491.0	15° C.	50'	3035.8	754.6	15° C.
36°	1861.7	294.9	T	46°	2432.1	494.8	T	56°	3046.5	759.6	T
10'	1870.9	297.7	E	10'	2441.9	498.7	E	10'	3057.2	764.6	E
20'	1880.1	300.6	.06	20'	2451.8	502.5	.10	20'	3067.9	769.7	.14
30'	1889.4	303.5	E	30'	2461.7	506.4	E	30'	3078.7	774.7	E
40'	1898.6	306.4	.013	40'	2471.5	510.3	.017	40'	3089.4	779.8	.017
50'	1907.9	309.3	15° C.	50'	2481.4	514.3	15° C.	50'	3100.2	784.9	15° C.
37°	1917.1	312.2	T	47°	2491.3	518.2	T	57°	3110.9	790.1	T
10'	1926.4	315.2	E	10'	2501.2	522.2	E	10'	3121.7	795.2	E
20'	1935.7	318.1	.06	20'	2511.2	526.1	.10	20'	3132.6	800.4	.14
30'	1945.0	321.1	E	30'	2521.1	530.1	E	30'	3143.4	805.6	E
40'	1954.3	324.1	.013	40'	2531.1	534.2	.017	40'	3154.2	810.9	.017
50'	1963.6	327.1	15° C.	50'	2541.0	538.2	15° C.	50'	3165.1	816.1	15° C.
38°	1972.9	330.2	T	48°	2551.0	542.2	T	58°	3176.0	821.4	T
10'	1982.2	333.2	E	10'	2561.0	546.3	E	10'	3186.9	826.7	E
20'	1991.5	336.3	.06	20'	2571.0	550.4	.10	20'	3197.8	832.0	.14
30'	2000.9	339.3	E	30'	2581.0	554.5	E	30'	3208.8	837.3	E
40'	2010.2	342.4	.013	40'	2591.0	558.6	.017	40'	3219.7	842.7	.017
50'	2019.6										

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=70°	I	T	E	I=80°	I	T	E	I=90°
61°	3375.0	920.2	+	71°	4086.9	1308.2	+	81°	4893.6	1805.3	+
10'	3386.3	925.9	5° C.	10'	4099.5	1315.6	5° C.	10'	4908.0	1814.7	5° C.
20'	3397.5	931.6	T	20'	4112.1	1322.9	T	20'	4922.5	1824.1	T
30'	3408.8	937.3	.25	30'	4124.8	1330.3	.30	30'	4937.0	1833.6	.36
40'	3420.1	943.1	E	40'	4137.4	1337.7	E	40'	4951.5	1843.1	E
50'	3431.4	948.9	.080	50'	4150.1	1345.1	.110	50'	4966.1	1852.6	.149
62°	3442.7	954.8	10° C.	72°	4162.8	1352.6	10° C.	82°	4980.7	1862.2	10° C.
10'	3454.1	960.6	T	10'	4175.6	1360.1	T	10'	4995.4	1871.8	T
20'	3465.4	966.5	.51	20'	4188.5	1367.6	.61	20'	5010.0	1881.5	.72
30'	3476.8	972.4	E	30'	4201.2	1375.2	E	30'	5024.8	1891.2	E
40'	3488.3	978.3	.159	40'	4214.0	1382.8	.220	40'	5039.5	1900.9	.299
50'	3499.7	984.3	15° C.	50'	4226.8	1390.4	15° C.	50'	5054.3	1910.7	15° C.
63°	3511.1	990.2	T	73°	4239.7	1398.0	T	83°	5069.2	1920.5	T
10'	3522.6	996.2	E	10'	4252.6	1405.7	E	10'	5084.0	1930.4	E
20'	3534.1	1002.3	.240	20'	4265.6	1413.5	.332	20'	5099.0	1940.3	.450
30'	3545.6	1008.3	T	30'	4278.5	1421.2	T	30'	5113.9	1950.3	T
40'	3557.2	1014.4	.159	40'	4291.5	1429.0	.220	40'	5128.9	1960.2	.299
50'	3568.7	1020.5	15° C.	50'	4304.6	1436.8	15° C.	50'	5143.9	1970.3	15° C.
64°	3580.3	1026.6	T	74°	4317.6	1444.6	T	84°	5159.0	1980.4	T
10'	3591.9	1032.8	E	10'	4330.7	1452.5	E	10'	5174.1	1990.5	E
20'	3603.5	1039.0	.240	20'	4343.8	1460.4	.332	20'	5189.3	2000.6	.450
30'	3615.1	1045.2	T	30'	4356.9	1468.4	T	30'	5204.4	2010.8	T
40'	3626.8	1051.4	.159	40'	4370.1	1476.4	.220	40'	5219.7	2021.1	.299
50'	3638.5	1057.7	15° C.	50'	4383.3	1484.4	15° C.	50'	5234.9	2031.4	15° C.
65°	3650.2	1063.9	T	75°	4396.5	1492.4	T	85°	5250.3	2041.7	T
10'	3661.9	1070.2	E	10'	4409.8	1500.5	E	10'	5265.6	2052.1	E
20'	3673.7	1076.6	.240	20'	4423.1	1508.6	.332	20'	5281.0	2062.5	.450
30'	3685.5	1082.9	T	30'	4436.4	1516.7	T	30'	5296.4	2073.0	T
40'	3697.2	1089.3	.159	40'	4449.7	1524.9	.220	40'	5311.9	2083.5	.299
50'	3709.0	1095.7	15° C.	50'	4463.1	1533.1	15° C.	50'	5327.4	2094.1	15° C.
66°	3720.9	1102.2	T	76°	4476.5	1541.4	T	86°	5343.0	2104.7	T
10'	3732.7	1108.6	E	10'	4489.9	1549.7	E	10'	5358.6	2115.3	E
20'	3744.6	1115.1	.240	20'	4503.4	1558.0	.332	20'	5374.2	2126.0	.450
30'	3756.5	1121.7	T	30'	4516.9	1566.3	T	30'	5389.9	2136.7	T
40'	3768.5	1128.2	.159	40'	4530.4	1574.7	.220	40'	5405.6	2147.5	.299
50'	3780.4	1134.8	15° C.	50'	4544.0	1583.1	15° C.	50'	5421.4	2158.4	15° C.
67°	3792.4	1141.4	T	77°	4557.6	1591.6	T	87°	5437.2	2169.2	T
10'	3804.4	1148.0	E	10'	4571.2	1600.1	E	10'	5453.1	2180.2	E
20'	3816.4	1154.7	.321	20'	4584.8	1608.6	.445	20'	5469.0	2191.1	.603
30'	3828.4	1161.3	T	30'	4598.5	1617.1	T	30'	5484.9	2202.2	T
40'	3840.5	1168.1	.159	40'	4612.2	1625.7	.220	40'	5500.9	2213.3	.299
50'	3852.6	1174.8	15° C.	50'	4626.0	1634.4	15° C.	50'	5517.0	2224.3	15° C.
68°	3864.7	1181.6	T	78°	4639.8	1643.0	T	88°	5533.1	2235.5	T
10'	3876.8	1188.4	E	10'	4653.6	1651.7	E	10'	5549.2	2246.7	E
20'	3889.0	1195.2	.240	20'	4667.4	1660.5	.332	20'	5565.4	2258.0	.450
30'	3901.2	1202.0	T	30'	4681.3	1669.2	T	30'	5581.6	2269.3	T
40'	3913.4	1208.9	.159	40'	4695.2	1678.1	.220	40'	5597.8	2280.6	.299
50'	3925.6	1215.8	15° C.	50'	4709.2	1686.9	15° C.	50'	5614.2	2292.0	15° C.
69°	3937.9	1222.7	T	79°	4723.2	1695.8	T	89°	5630.5	2303.5	T
10'	3950.2	1229.7	E	10'	4737.2	1704.7	E	10'	5646.9	2315.0	E
20'	3962.5	1236.7	.240	20'	4751.2	1713.7	.332	20'	5663.4	2326.6	.450
30'	3974.8	1243.7	T	30'	4765.3	1722.7	T	30'	5679.9	2338.2	T
40'	3987.2	1250.8	.159	40'	4779.4	1731.7	.220	40'	5696.4	2349.8	.299
50'	3999.5	1257.9	15° C.	50'	4793.6	1740.8	15° C.	50'	5713.0	2361.5	15° C.
70°	4011.9	1265.0	T	80°	4807.7	1749.9	T	90°	5729.7	2373.3	T
10'	4024.4	1272.1	E	10'	4822.0	1759.0	E	10'	5746.3	2385.1	E
20'	4036.8	1279.3	.159	20'	4836.2	1768.2	.184	20'	5763.1	2397.0	.220
30'	4049.3	1286.5	T	30'	4850.5	1777.4	T	30'	5779.9	2408.9	T
40'	4061.8	1293.6	.159	40'	4864.8	1786.7	.220	40'	5796.7	2420.9	.299
50'	4074.4	1300.9	.485	50'	4879.2	1796.0	.671	50'	5813.6	2432.9	.910

T = R tan ½ I

E = R exsec ½ I

TABLE IX. TANGENTS AND EXTERNALS TO A 1° CURVE

I	T	E	I=100°	I	T	E	I=110°	I	T	E	I=120°
91°	5330.5	2444.9	+	101°	6950.6	3278.1	+	111°	8336.7	4386.1	+
10'	5347.5	2457.1	5° C.	10'	6971.3	3294.1	5° C.	10'	8362.7	4407.6	5° C.
20'	5364.6	2469.3	T	20'	6992.0	3310.1	T	20'	8388.9	4429.2	T
30'	5381.7	2481.5	.43	30'	7012.7	3326.1	.51	30'	8415.1	4450.9	.62
40'	5398.8	2493.8	E	40'	7033.6	3342.3	E	40'	8441.5	4472.7	E
50'	5916.0	2506.1	.200	50'	7054.5	3358.5	.268	50'	8468.0	4494.6	.360
92°	5933.2	2518.5	10° C.	102°	7075.5	3374.9	10° C.	112°	8494.6	4516.6	10° C.
10'	5950.5	2531.0	T	10'	7096.6	3391.2	T	10'	8521.3	4538.8	T
20'	5967.9	2543.5	.86	20'	7117.8	3407.7	.103	20'	8548.1	4561.1	.125
30'	5985.3	2556.0	E	30'	7139.0	3424.3	E	30'	8575.0	4583.4	E
40'	6002.7	2568.6	.401	40'	7160.3	3440.9	.536	40'	8602.1	4606.0	.621
50'	6020.2	2581.3	10° C.	50'	7181.7	3457.6	10° C.	50'	8629.3	4628.6	10° C.
93°	6037.8	2594.0	T	103°	7203.2	3474.4	T	113°	8656.6	4651.3	T
10'	6055.4	2606.8	E	10'	7224.7	3491.3	E	10'	8684.0	4674.2	E
20'	6073.1	2619.7	.86	20'	7246.3	3508.2	.103	20'	8711.5	4697.2	.125
30'	6090.8	2632.6	E	30'	7268.0	3525.2	E	30'	8739.2	4720.3	E
40'	6108.6	2645.5	.401	40'	7289.8	3542.4	.536	40'	8767.0	4743.6	.621
50'	6126.4	2658.5	10° C.	50'	7311.7	3559.6	10° C.	50'	8794.9	4766.9	10° C.
94°	6144.3	2671.6	T	104°	7333.6	3576.8	T	114°	8822.9	4790.4	T
10'	6162.2	2684.7	E	10'	7355.6	3594.2	E	10'	8851.0	4814.1	E
20'	6180.2	2697.9	.86	20'	7377.8	3611.7	.103	20'	8879.3	4837.8	.125
30'	6198.3	2711.2	E	30'	7399.9	3629.2	E	30'	8907.7	4861.7	E
40'	6216.4	2724.5	.401	40'	7422.2	3646.8	.536	40'	8936.3	4885.7	.621
50'	6234.6	2737.9	10° C.	50'	7444.6	3664.5	10° C.	50'	8965.0	4909.9	10° C.
95°	6252.8	2751.3	T	105°	7467.0	3682.3	T	115°	8993.8	4934.1	T
10'	6271.1	2764.8	E	10'	7489.6	3700.2	E	10'	9022.7	4958.6	E
20'	6289.4	2778.3	.86	20'	7512.2	3718.2	.103	20'	9051.7	4983.1	.125
30'	6307.9	2792.0	E	30'	7534.9	3736.2	E	30'	9080.9	5007.8	E
40'	6326.3	2805.6	.401	40'	7557.7	3754.4	.536	40'	9110.3	5032.6	.621
50'	6344.8	2819.4	10° C.	50'	7580.5	3772.6	10° C.	50'	9139.8	5057.6	10° C.
96°	6363.4	2833.7	T	106°	7603.5	3791.0	T	116°	9169.4	5082.7	T
10'	6382.1	2847.0	E	10'	7626.6	3809.4	E	10'	9199.1	5107.9	E
20'	6400.8	2861.0	.86	20'	7649.7	3827.9	.103	20'	9229.0	5133.3	.125
30'	6419.5	2875.0	E	30'	7672.9	3846.5	E	30'	9259.0	5158.8	E
40'	6438.4	2889.0	.401	40'	7696.3	3865.2	.536	40'	9289.2	5184.5	.621
50'	6457.3	2903.1	10° C.	50'	7719.7	3884.0	10° C.	50'	9319.5	5210.3	10° C.
97°	6476.2	2917.3	T	107°	7743.2	3902.9	T	117°	9349.9	5236.2	T
10'	6495.2	2931.6	E	10'	7766.8	3921.9	E	10'	9380.5	5262.3	E
20'	6514.3	2945.9	.86	20'	7790.5	3940.9	.103	20'	9411.3	5288.6	.125
30'	6533.4	2960.3	E	30'	7814.3	3960.1	E	30'	9442.2	5315.0	E
40'	6552.6	2974.7	.401	40'	7838.1	3979.4	.536	40'	9473.2	5341.5	.621
50'	6571.9	2989.2	10° C.	50'	7862.1	3998.7	10° C.	50'	9504.4	5368.2	10° C.
98°	6591.2	3003.8	T	108°	7886.2	4018.2	T	118°	9535.7	5395.1	T
10'	6610.6	3018.4</									

TABLE X.
MIDDLE ORDINATES OF RAILS
Length of Rail (feet)

C	R	30	28	26	24	22	20	C	R	30	28	26	24	22	20
o /	Feet	Inch	Inch	Inch	Inch	Inch	Inch	o	Feet	Inch	Inch	Inch	Inch	Inch	Inch
0-20	17189	.08	.07	.06	.05	.04	.03	8	716.8	1.88	1.64	1.42	1.20	1.01	.84
0-40	8594	.16	.14	.12	.10	.08	.07	9	637.3	2.12	1.84	1.60	1.35	1.14	.94
1-0	5730	.24	.20	.18	.15	.13	.10	10	573.7	2.36	2.05	1.78	1.50	1.27	1.04
1-20	4297	.31	.27	.23	.20	.17	.13	11	521.7	2.59	2.26	1.95	1.65	1.39	1.15
1-40	3438	.39	.34	.29	.25	.21	.17	12	478.3	3.83	2.47	2.15	1.81	1.54	1.26
2-0	2865	.47	.41	.35	.30	.25	.20	13	441.7	3.05	2.66	2.30	1.96	1.66	1.36
2-20	2456	.55	.48	.41	.35	.29	.23	14	410.3	3.30	2.87	2.48	2.10	1.78	1.46
2-40	2149	.63	.55	.47	.40	.33	.27	15	383.1	3.54	3.08	2.68	2.26	1.91	1.57
3-0	1910	.71	.62	.53	.45	.38	.31	16	359.3	3.76	3.28	2.83	2.40	2.04	1.67
3-20	1719	.78	.68	.59	.50	.42	.35	17	338.3	4.00	3.48	3.02	2.57	2.16	1.78
3-40	1563	.86	.75	.65	.55	.46	.38	18	319.6	4.21	3.67	3.18	2.70	2.28	1.87
4-0	1433	.94	.82	.71	.60	.50	.42	19	302.9	4.45	3.89	3.36	2.86	2.41	1.98
4-20	1323	1.02	.89	.77	.65	.55	.45	20	287.9	4.70	4.09	3.55	3.00	2.54	2.09
4-40	1228	1.10	.96	.83	.70	.59	.48	22	262.0	5.16	4.44	3.84	3.30	2.80	2.29
5	1146	1.18	1.03	.89	.75	.63	.52	24	240.5	5.64	4.92	4.20	3.59	3.04	2.50
6	955.3	1.41	1.23	1.06	.90	.76	.62	26	222.3	6.07	5.29	4.58	3.88	3.29	2.70
7	819.0	1.65	1.44	1.24	1.05	.89	.73								

TABLE XI.
SHORT RADIUS CURVES

Radius Feet	Chord Feet	Central Angle	Deflection	Deflection for 1 Foot
35	10	16-26	8-13	49.3
45	10	12-46	6-23	38.3
50	15	17-16	8-38	34.5
60	15	14-22	7-11	28.8
75	15	11-30	5-45	23.0
100	20	11-30	5-45	17.3
120	20	9-34	4-47	14.3
150	20	7-39	3-49	11.5
190	25	7-32	3-46	9.15
200	25	7-10	3-35	8.6
225	25	6-25	3-12	7.7
240	25	5-58	2-59	7.2
250	25	5-44	2-52	6.9
275	25	5-12	2-36	6.2
288	50	9-58	4-59	6.0
300	50	9-32	4-46	5.7
350	50	8-12	4-06	4.9
376	50	7-40	3-50	4.6
400	50	7-10	3-35	4.3
410	50	7-00	3-30	4.2

To find length of curve divide angle from P. C. to P. T. by central angle of chord and multiply by length of chord.

TABLE XII.
INCLINED DISTANCE OF 100 FT. REDUCED TO HORIZONTAL

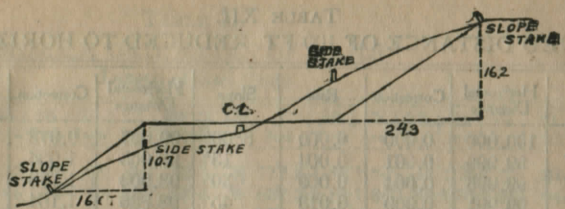
Slope	Horizontal Distance	Correction	Rise	Slope	Horizontal Distance	Correction	Rise
0°00'	100.000	0.000	0.000	8°00'	99.027	0.973	0.139
15'	99.999	0.001	0.004	15'	98.965	1.035	0.143
30'	99.996	0.004	0.009	30'	98.902	1.098	0.148
45'	99.991	0.009	0.013	45'	98.836	1.164	0.152
1 00	99.985	0.015	0.017	9 00	98.769	1.231	0.156
15	99.976	0.024	0.022	15	98.700	1.300	0.161
30	99.966	0.034	0.026	30	98.629	1.371	0.165
45	99.953	0.047	0.031	45	98.556	1.444	0.169
2 00	99.939	0.061	0.035	10 00	98.481	1.519	0.174
15	99.923	0.077	0.039	15	98.404	1.596	0.178
30	99.905	0.095	0.044	30	98.325	1.675	0.182
45	99.885	0.115	0.048	45	98.245	1.755	0.187
3 00	99.863	0.137	0.052	11 00	98.163	1.837	0.191
15	99.839	0.161	0.057	15	98.079	1.921	0.195
30	99.813	0.187	0.061	30	97.992	2.008	0.199
45	99.786	0.214	0.065	45	97.905	2.095	0.204
4 00	99.756	0.244	0.070	12 00	97.815	2.185	0.208
15	99.725	0.275	0.074	15	97.723	2.277	0.212
30	99.692	0.308	0.078	30	97.630	2.370	0.216
45	99.657	0.343	0.083	45	97.534	2.466	0.221
5 00	99.619	0.381	0.087	13 00	97.437	2.563	0.225
15	99.580	0.420	0.092	15	97.338	2.662	0.229
30	99.540	0.460	0.096	30	97.237	2.763	0.233
45	99.497	0.503	0.100	45	97.134	2.866	0.238
6 00	99.452	0.548	0.105	14 00	97.030	2.970	0.242
15	99.406	0.594	0.109	15	96.923	3.077	0.246
30	99.357	0.643	0.113	30	96.815	3.185	0.250
45	99.307	0.693	0.118	45	96.705	3.295	0.255
7 00	99.255	0.745	0.122	15 00	96.593	3.407	0.259
15	99.200	0.800	0.126	15	96.479	3.521	0.263
30	99.144	0.856	0.131	30	96.363	3.637	0.267
45	99.087	0.913	0.135	45	96.246	3.754	0.271

For each foot take one one-hundredth of each reading.

TABLE XIII.
MINUTES IN DECIMALS OF A DEGREE.

0 30"	.00833	10' 30"	.17500	20' 30"	.34167	30' 10"	.50833	40' 30"	.67500	50' 10"	.84167
1 00	.01667	11 00	.18333	21 00	.35000	31 00	.51667	41 00	.68333	51 00	.85000
30	.02500	30	.19167	30	.35833	30	.52500	30	.69167	30	.85833
2 00	.03333	12 00	.20000	22 00	.36667	32 00	.53333	42 00	.70000	52 00	.86667
30	.04167	30	.20833	30	.37500	30	.54167	30	.70833	30	.87500
3 00	.05000	13 00	.21667	23 00	.38333	33 00	.55000	43 00	.71667	53 00	.88333
30	.05833	30	.22500	30	.39167	30	.55833	30	.72500	30	.89167
4 00	.06667	14 00	.23333	24 00	.40000	34 00	.56667	44 00	.73333	54 00	.90000
30	.07500	30	.24167	30	.40833	30	.57500	30	.74167	30	.90833
5 00	.08333	15 00	.25000	25 00	.41667	35 00	.58333	45 00	.75000	55 00	.91667
30	.09167	30	.25833	30	.42500	30	.59167	30	.75833	30	.92500
6 00	.10000	16 00	.26667	26 00	.43333	36 00	.60000	46 00	.76667	56 00	.93333
30	.10833	30	.27500	30	.44167	30	.60833	30	.77500	30	.94167
7 00	.11667	17 00	.28333	27 00	.45000	37 00	.61667	47 00	.78333	57 00	.95000
30	.12500	30	.29167	30	.45833	30	.62500	30	.79167	30	.95833
8 00	.13333	18 00	.30000	28 00	.46667	38 00	.63333	48 00	.80000	58 00	.96667
30	.14167	30	.30833	30	.47500	30	.64167	30	.80833	30	.97500
9 00	.15000	19 00	.31667	29 00	.48333	39 00	.65000	49 00	.81667	59 00	.98333
30	.15833	30	.32500	30	.49167	30	.65833	30	.82500	30	.99167
10 00	.16667	20 00	.33333	30 00	.50000	40 00	.66667	50 00	.83333	60 00	1.00000

C
0 / I
0-20
0-40
1-0
1-20
1-40
2-0
2-20
2-40
3-0
3-20
3-40
4-0
4-20
4-40
5
6
7



DISTANCES FROM SIDE STAKES FOR CROSS-SECTIONING.

SLOPE 1 1/2 TO 1. ROADWAY OF ANY WIDTH.

	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	
0	0 00	0 15	0 30	0 45	0 60	0 75	0 90	1 05	1 20	1 35	0
1	1 50	1 05	1 20	1 35	1 50	1 65	1 80	1 95	2 10	2 25	1
2	3 00	3 15	3 30	3 45	3 60	3 75	3 90	4 05	4 20	4 35	2
3	4 50	4 65	4 80	4 95	5 10	5 25	5 40	5 55	5 70	5 85	3
4	6 00	6 15	6 30	6 45	6 60	6 75	6 90	7 05	7 20	7 35	4
5	7 50	7 65	7 80	7 95	8 10	8 25	8 40	8 55	8 70	8 85	5
6	9 00	9 15	9 30	9 45	9 60	9 75	9 90	10 05	10 20	10 35	6
7	10 50	10 65	10 80	10 95	11 10	11 25	11 40	11 55	11 70	11 85	7
8	12 00	12 15	12 30	12 45	12 60	12 75	12 90	13 05	13 20	13 35	8
9	13 50	13 65	13 80	13 95	14 10	14 25	14 40	14 55	14 70	14 85	9
10	15 00	15 15	15 30	15 45	15 60	15 75	15 90	16 05	16 20	16 35	10
11	16 50	16 65	16 80	16 95	17 10	17 25	17 40	17 55	17 70	17 85	11
12	18 00	18 15	18 30	18 45	18 60	18 75	18 90	19 05	19 20	19 35	12
13	19 50	19 65	19 80	19 95	20 10	20 25	20 40	20 55	20 70	20 85	13
14	21 00	21 15	21 30	21 45	21 60	21 75	21 90	22 05	22 20	22 35	14
15	22 50	22 65	22 80	22 95	23 10	23 25	23 40	23 55	23 70	23 85	15
16	24 00	24 15	24 30	24 45	24 60	24 75	24 90	25 05	25 20	25 35	16
17	25 50	25 65	25 80	25 95	26 10	26 25	26 40	26 55	26 70	26 85	17
18	27 00	27 15	27 30	27 45	27 60	27 75	27 90	28 05	28 20	28 35	18
19	28 50	28 65	28 80	28 95	29 10	29 25	29 40	29 55	29 70	29 85	19
20	30 00	30 15	30 30	30 45	30 60	30 75	30 90	31 05	31 20	31 35	20
21	31 50	31 65	31 80	31 95	32 10	32 25	32 40	32 55	32 70	32 85	21
22	33 00	33 15	33 30	33 45	33 60	33 75	33 90	34 05	34 20	34 35	22
23	34 50	34 65	34 80	34 95	35 10	35 25	35 40	35 55	35 70	35 85	23
24	36 00	36 15	36 30	36 45	36 60	36 75	36 90	37 05	37 20	37 35	24
25	37 50	37 65	37 80	37 95	38 10	38 25	38 40	38 55	38 70	38 85	25
26	39 00	39 15	39 30	39 45	39 60	39 75	39 90	40 05	40 20	40 35	26
27	40 50	40 65	40 80	40 95	41 10	41 25	41 40	41 55	41 70	41 85	27
28	42 00	42 15	42 30	42 45	42 60	42 75	42 90	43 05	43 20	43 35	28
29	43 50	43 65	43 80	43 95	44 10	44 25	44 40	44 55	44 70	44 85	29
30	45 00	45 15	45 30	45 45	45 60	45 75	45 90	46 05	46 20	46 35	30
31	46 50	46 65	46 80	46 95	47 10	47 25	47 40	47 55	47 70	47 85	31
32	48 00	48 15	48 30	48 45	48 60	48 75	48 90	49 05	49 20	49 35	32
33	49 50	49 65	49 80	49 95	50 10	50 25	50 40	50 55	50 70	50 85	33
34	51 00	51 15	51 30	51 45	51 60	51 75	51 90	52 05	52 20	52 35	34
35	52 50	52 65	52 80	52 95	53 10	53 25	53 40	53 55	53 70	53 85	35
36	54 00	54 15	54 30	54 45	54 60	54 75	54 90	55 05	55 20	55 35	36
37	55 50	55 65	55 80	55 95	56 10	56 25	56 40	56 55	56 70	56 85	37
38	57 00	57 15	57 30	57 45	57 60	57 75	57 90	58 05	58 20	58 35	38
39	58 50	58 65	58 80	58 95	59 10	59 25	59 40	59 55	59 70	59 85	39
40	60 00	60 15	60 30	60 45	60 60	60 75	60 90	61 05	61 20	61 35	40
41	61 50	61 65	61 80	61 95	62 10	62 25	62 40	62 55	62 70	62 85	41
42	63 00	63 15	63 30	63 45	63 60	63 75	63 90	64 05	64 20	64 35	42
43	64 50	64 65	64 80	64 95	65 10	65 25	65 40	65 55	65 70	65 85	43
44	66 00	66 15	66 30	66 45	66 60	66 75	66 90	67 05	67 20	67 35	44
45	67 50	67 65	67 80	67 95	68 10	68 25	68 40	68 55	68 70	68 85	45
46	69 00	69 15	69 30	69 45	69 60	69 75	69 90	70 05	70 20	70 35	46
47	70 50	70 65	70 80	70 95	71 10	71 25	71 40	71 55	71 70	71 85	47
48	72 00	72 15	72 30	72 45	72 60	72 75	72 90	73 05	73 20	73 35	48
49	73 50	73 65	73 80	73 95	74 10	74 25	74 40	74 55	74 70	74 85	49
50	75 00	75 15	75 30	75 45	75 60	75 75	75 90	76 05	76 20	76 35	50

Computed by L. Leland Locke.

475
582
413
250
276
344
601
680
482
910.3
29.77
31.76
56.53
41.03
15.50

To find

